PV MODULES FOR GROUND TESTING CR 179476

NAS3-24657

FINAL REPORT

Prepared for

NASA-Lewis Research Center Cleveland, OH 44135

by

Lockheed Missiles & Space Company, Inc.
Sunnyvale, CA 94088

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FOREWORD

This report documents the work performed by Lockheed Missiles & Space Co., Inc., Sunnyvale, California, for the Lewis Research Center of the National Aeronautics and Space Administration under contract no. NAS3-24657 on the PV Modules for Ground Testing.

The term of this contract was 4.5 months beginning on 8 August 1985 and concluding on 20 January 1986. This report summarizes the full term effort performed on the subject contract over this entire period. The outcome of this contract was four solar cell test modules which will be tested in a plasma chamber to investigate current loss mechanisms. Henry Curtis of the Power Systems Branch of NASA/LeRC provided technical direction for this work.

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1.0 INTRODUCTION

Increased power requirements for missions in the 1990's will provide the impetus for higher solar array operating voltages. Weight reductions for both cable harnessing and converters will be realized at these higher voltages. However, operation in regions of high plasma density at high voltage could significantly offset any weight savings. In order to realistically assess the performance potential of high voltage solar arrays, the question of the magnitude of the power loss associated with plasma interaction must be answered.

A solar array in space will be surrounded by a plasma sheath. This sheath is the region in which the potential changes from that of the exposed conductors or charged dielectrics on the array to that of the plasma. In general, the current collected by the array will depend upon the voltage, plasma particle density and energy, and the array geometry. Additional factors contributing to current collection include (a) motion of the spacecraft relative to the plasma for heavy ion collection, (b) the earth's magnetic field, (c) potential distribution upon the array, and (d) material properties of the array.

1.1 OBJECTIVE

The main objective of this contract was to design and build a minimum of three photovoltaic test panels for plasma interaction experiments. These experiments are intended to provide data on the interactions between high-voltage solar arrays and the space plasma environment. Data gathered will significantly contribute to the development of design criteria for the space station solar arrays. Electrical isolation between the solar cell strings and the module mounting plate is required for high-voltage bias.

1.2 SCOPE

LMSC is contractually obligated to supply three different solar cell module types utilizing 0.020-0.030 cm (8-12 mils) thick, 2 ohm-cm, silicon solar cells. Interconnected cell series strings must demonstrate an electrical conversion efficiency

of at least 11.0% at 1 AMO and 28 degrees Celsius. Further electrical requirements include a capacitance range of 2000-2500 pf and a resistance greater than 10^{11} ohms between the cells and the module plate. Three 0.91 m (3 ft.) 22 guage Kapton coated copper wire leads exiting from one of the short sides of the plate are required.

In addition to the three different solar cell module types which LMSC was under contract to deliver, a fourth module, utilizing 8×8 cm silicon solar cell technology was furnished. A brief description of each of the different module types delivered is given below:

Module	P/N	Description
1	x8512604-501	0.020 cm (0.008 in.) thick, 5.9 x 5.9 cm Si cells, gridded back, wrap-around contacts, 0.013 cm (0.005 in.) thick individual CMX covers, welded Cu/Kapton flexible interconnects, cells are bonded to module plate face up, 28 cells in series
2	x8512604-503	Same as module type #1 except cells are bonded to module plate face down
3	x8517165-501	Same as module #1 except BSR cell and conventional n-bar contact with soldered Ag plated/Mo interconnect
4	x8517166-501	0.020 cm (0.008 in.) thick, 8 x 8 cm Si cells, gridded back, wrap-through contacts, 0.053 cm (0.021 in.) CMX superstrate, welded Cu/Kapton flexible interconnect, cells are bonded to module plate face up, 15 cells in series

2.0 TECHNICAL PROGRESS SUMMARY

The contract was initiated within LMSC during mid August 1985 and completed with the delivery of four solar cell module plates to LeRC in January 1986. A complete contract master schedule is shown in Figure 1.

2.1 TASK 1 - DESIGN AND ANALYSIS

During this task, preliminary engineering drawings were released for procurement of all long lead time items. In addition, adhesive bond evaluation tests were conducted at this time to determine bond strength between FM73M adhesive and a non-acid etched, MIL-C-5541 coated aluminum alloy surface. The flat-wise tensile test set-up employed to evaluate bond strength is shown in Figure 2.

Test results, summarized in Table 1, show that FM73M forms a strong bond to MIL-C-5541 coated aluminum alloy. All bond failures occurred at the unprimed interface. The failure mechanism was primarily cohesive. The use of BR 127 primer gave additional bond strength to the chemically coated aluminum/FM73M bond. The average tensile strength of the samples tested (35.4 MPa/5146 psi) compares favorably to an acid etched aluminum surface/FM73M bond (41.4 MPa/6000 psi). Results from this test were incorporated in the fabrication of the aluminum plate assembly (x8512607) as seen on the engineering drawing attached in Appendix A.

2.2 TASK 2 - MODULE FABRICATION

Electrical evaluation tests were performed on "one cell" models (shown in Figure 3) of the three solar cell modules. The purpose of these tests were to verify compliance with the design requirements for resistance greater than 10^{11} ohms and capacitance within the 2000-2500 pf range between solar cells and the module plate. A linear scale-up factor was assumed to predict full scale module capacitance. Fringing field effects at the solar cell edges was neglected since intercell spacing was small compared to capacitor plate spacing.

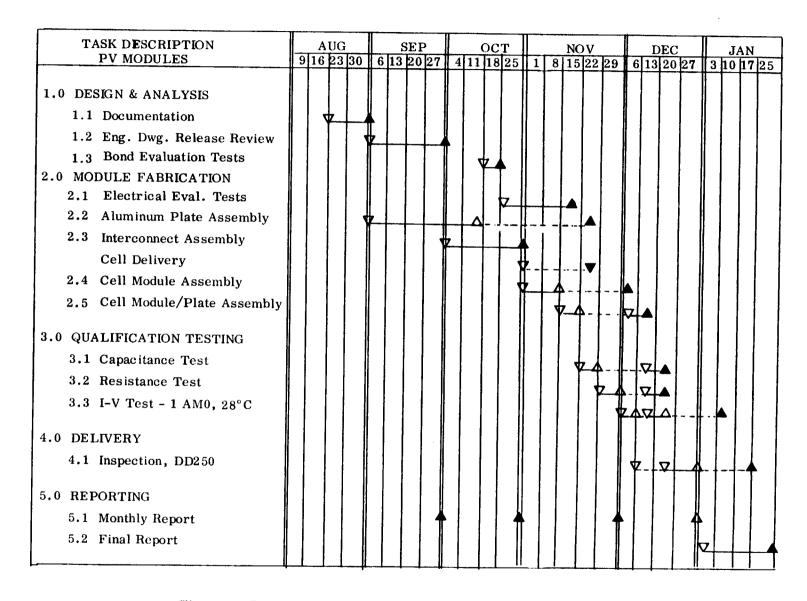


Figure 1 PV Modules for Ground Testing - Master Schedule

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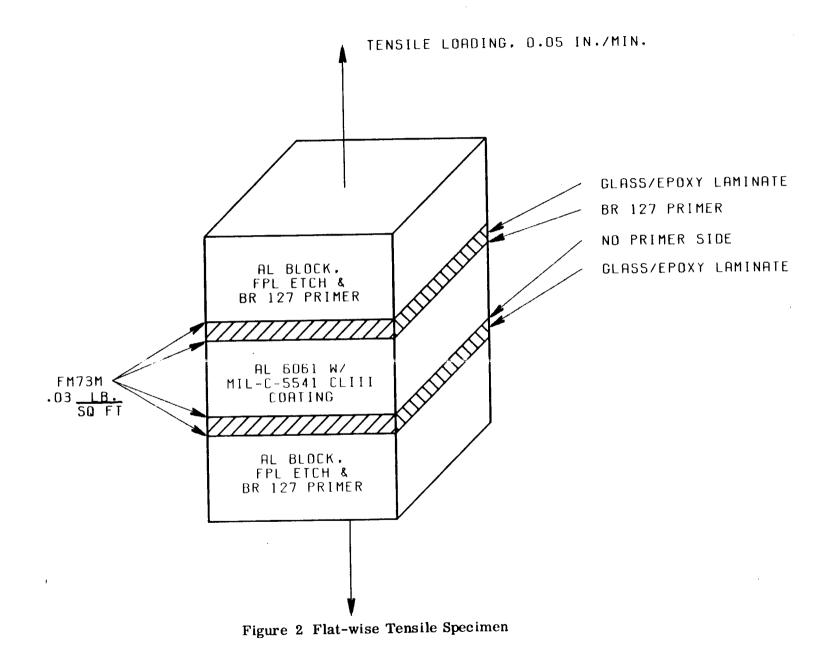


TABLE 1
FLATWISE TENSILE RESULTS

SPECIMEN	TENSILE, PSI	MODE OF FAILURE (1)
1(2)	6073	80% COHESIVE, 20% GLASS DELAM
2	5094	75% COHESIVE, 15% GLASS DELAM, 10% ADHESIVE TO A1 (NON PRIMED SIDE
3	4767	90% COHESIVE, 10% ADHESIVE TO AI
4	4310	95% COHESIVE, 5% ADHESIVE TO AI
5	5486	80% COHESIVE, 10% ADHESIVE TO AI, 10% GLASS DELAM
	AVG = 5146	
ll failures occurred	at Al without primer interface.	

⁽²⁾ Specimen loaded to 3600 psi and released due to load pin deflection. Specimen was tested to failure using a new pin.

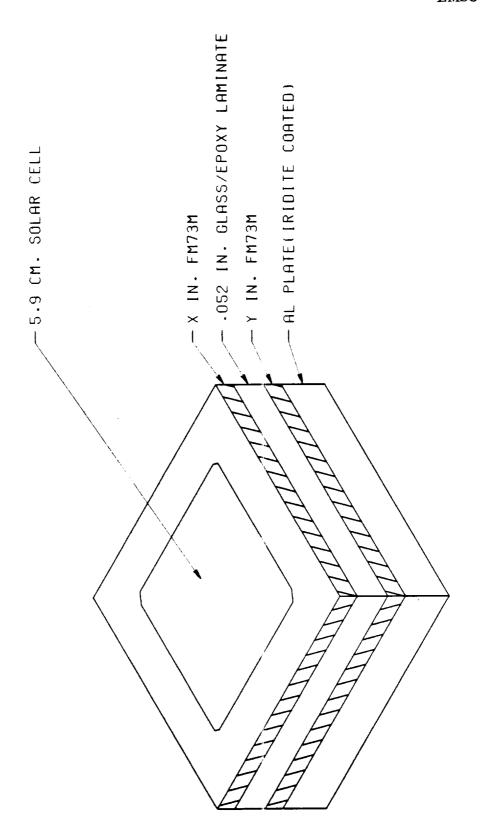


Figure 3 "One-Cell" Electrical Model

Preliminary calculations (see Appendix B) had suggested a dielectric stack of: 0.013 cm (0.005 in.) thick epoxy adhesive, 0.132 cm (0.052 in.) thick glass epoxy laminate, 0.005 cm (0.002 in.) thick silicone adhesive and a 0.002 cm (0.001 in.) thick Kapton film to meet the electrical design requirements. Test results, summarized in Table 2, show that an additional 0.038 cm (0.015 in.) thick layer of epoxy dielectric is needed to approach the electrical design requirements (sample #5). The inaccuracy of the dielectric thickness calculations can be attributed to the approximate and directional nature of the constants used in the preliminary calculations. The added dielectric thickness was incorporated into the design by the addition of FM73M adhesive layers onto the face of the glass/epoxy laminate. A photograph of the "one cell test" samples is shown in Figure 4.

Upon completion of all testing, hardware fabrication was initiated. Photographic documentation of all completed hardware is shown in Figures 5 through 11.

2.3 TASK 3 - QUALIFICATION TESTING

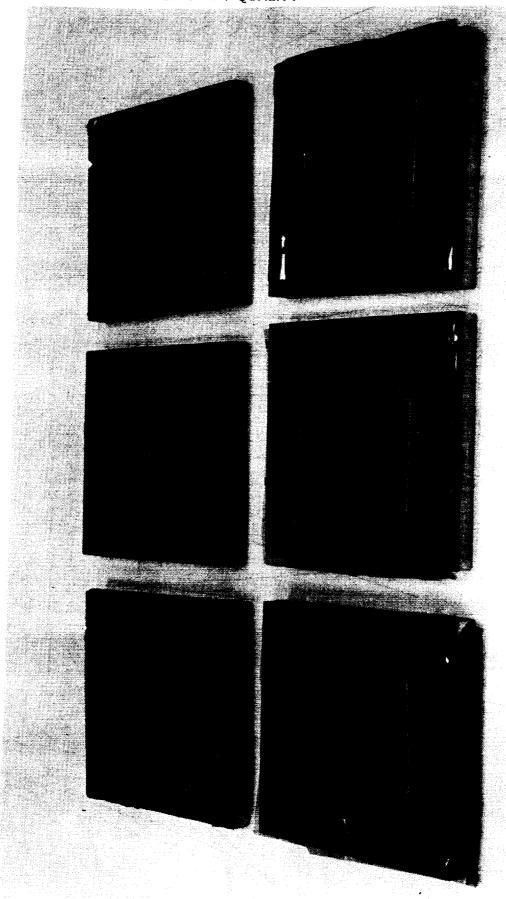
Results of capacitance and resistance testing of the full scale solar cell modules is summarized in Table 3. Module Type 4 (x8517166-501) was shown to exhibit a comparatively low capacitance of 1100 pf and a low resistance between cell and mounting plate of 8×10^{11} ohms. In addition, module type 2 (x8512604-503). exhibits a capacitance below the required range, probably as a result of the extra thickness of dielectric (coverglass) in the stack. These results do not comply with the contract requirements, however, approval for hardware delivery was given by the contract monitor.

All modules were shown to exhibit an electrical conversion efficiency greater than 11%. Electrical I-V curves are provided in Figures 12 through 18 at 28 degrees Celcius and 1 AMO. It should be noted that Figures 12 through 14 show the I-V characteristics of the solar cell modules before being bonded to the mounting plate. Particular attention should be brought to Figure 13 which is taken as baseline for module type 2 (x8512604-503) rather than Figure 16 which shows the solar cell I-V characteristics when illuminated from the backside only. Thus the electrical conversion efficiencies listed in Table 3 are from Figures 15, 13, 17, and 18

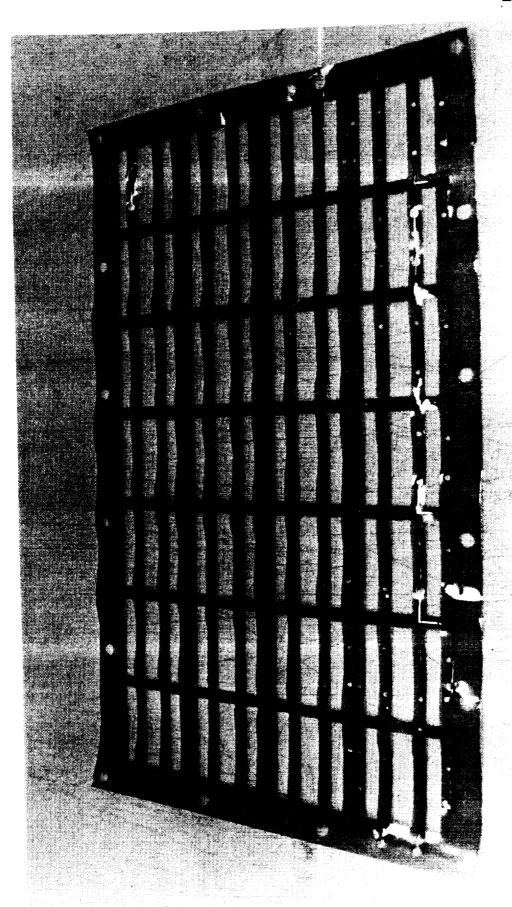
TABLE 2
CAPACITANCE/RESISTANCE TEST RESULTS

Sample No.	Description	Capacitance (pf) Measured for "One Cell" Model*	Capacitance (pf) Extrapolated to Full Scale Model	Resistance (ohm) at 500V**
1	Module Type #1 (Cells Bonded Face Up) X = 0 Y = .005	102.2	2786	1.2 x 10 ¹¹
2	Module Type #2 (Cells Bonded Face Down) X = 0 Y = .005	98.5	27 58	1.2 x 10 ¹¹
3	Module Type #3 Conventional N-Bar Cells Bonded Face Up X = 0 Y = .005	94.6	2649	3.1 x 10 ¹⁰
4	Module Type #1 (Cells Bonded Face Up) X = .010 Y = .005	89.6	2508	4.5 x 10 ¹¹
5	Module Type #1 (Cells Bonded Face Up) X = .010 Y = .010	84.7	2400	1.8 x 10 ¹¹
6	Module Type #1 (Cells Bonded Face Up) X = .015 Y = .010	73.4	2054	2.6 x 10 ¹¹

Measured by: *HP4274A Multi Frequency LCR Meter (LMSC #121867)
**1620C Megohmeter, Freed Xfmr Co. (MSL #60668)



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11 LOCKHEED MISSILES & SPACE COMPANY, INC.

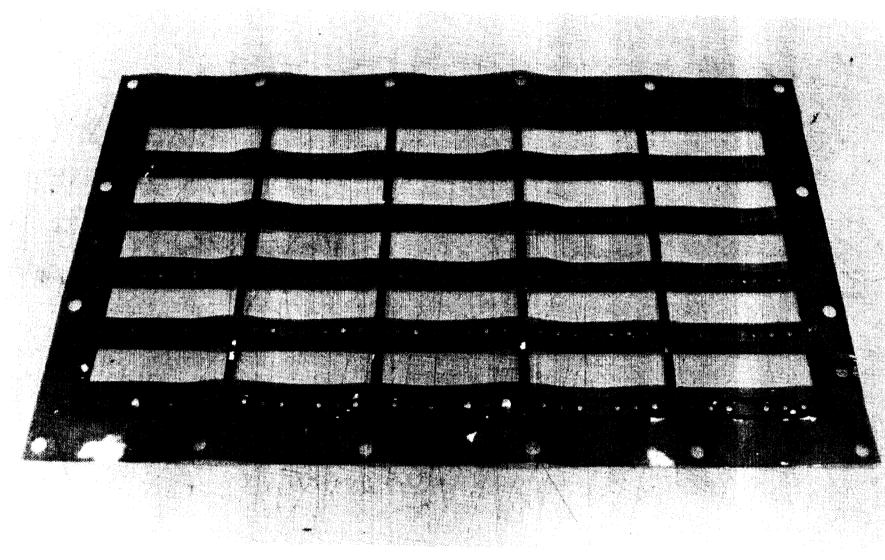
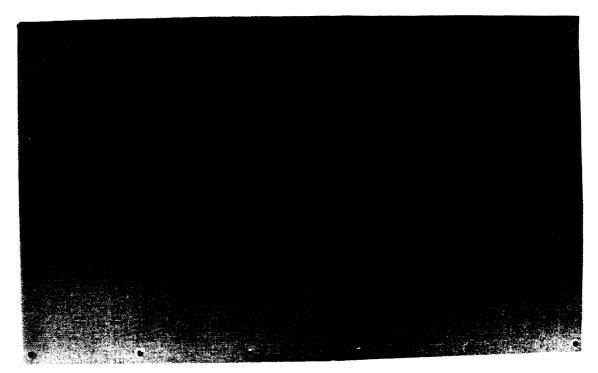
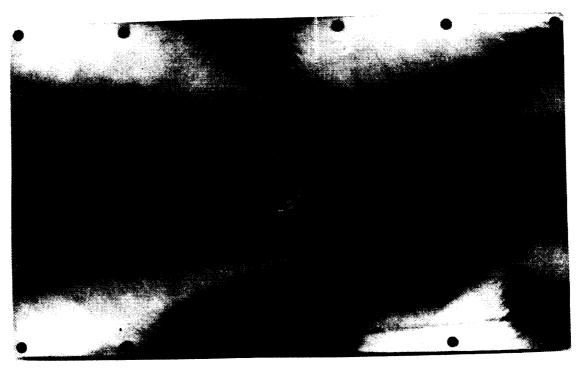


Figure 6 Circuit Assembly 8 x 8 cm Cells x8517161-501

LOCKHEED MISSILES & SPACE COMPANY. INC.



(Front Side)



(Back Side)

Figure 7 Aluminum Plate Assembly (X8512607-501)



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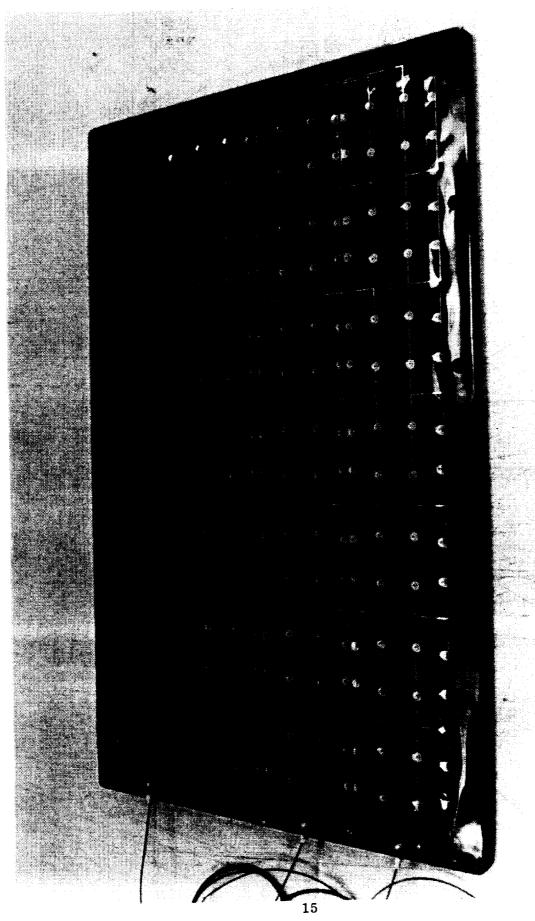


Figure 9 Module/Plate Assembly x8512604-503

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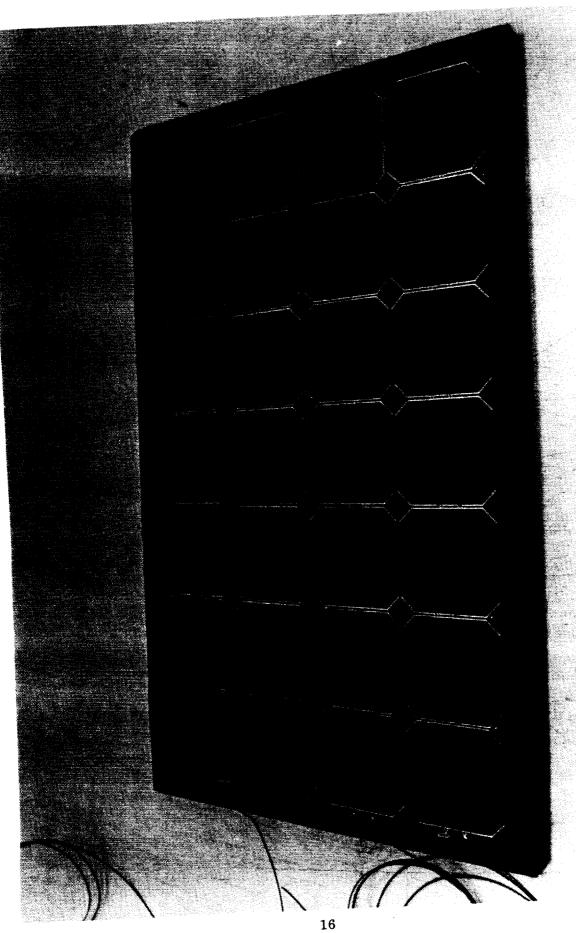


Figure 10 Module/Plate Assembly (Conventional) x8517165-501

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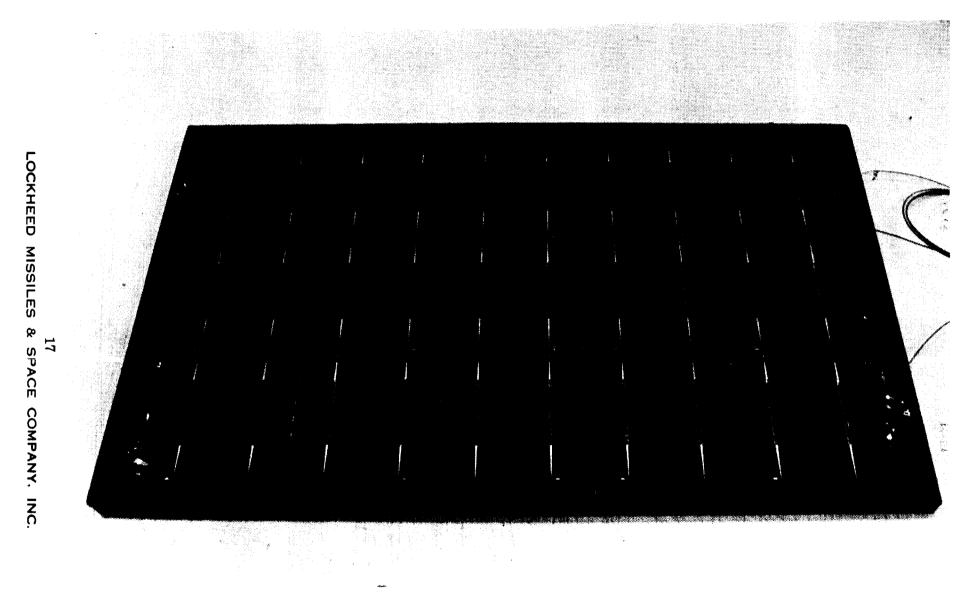


Figure 11 Module/Plate Assembly (8 x 8 cm Cells) x8517166-501

MSC-D973480

TABLE 3
ELECTRICAL SUMMARY

PV MODULE P/N	*CAPACITANCE (pf) (at 100 Hz)	**RESISTANCE (Ω) (at 500V)	ELECTRICAL CONVERSION EFFICIENCY (%) (at T = 28°C)
X8512604-501	2010	1.2×10^{11}	11.72
X8512604-503	1880	2.0 x 10 ¹¹	11.22
X8517165-501	2070	1.6 x 10 ¹¹	12.06
X8517166-501	1100	8.0 x 10 ¹⁰	11.31

MEASURED BY: *HP4274A MULTI-FREQUENCY LCR METER (LMSC #121867)
**1620C MEGOHMETER, FREED XFMR CO. (MSL #60668)

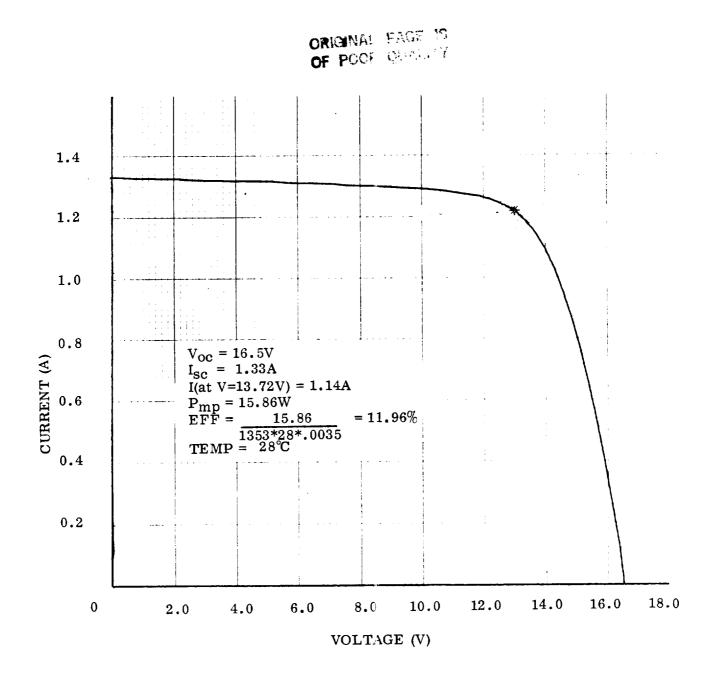


Figure 12 I-V Curve (X8517162-001)

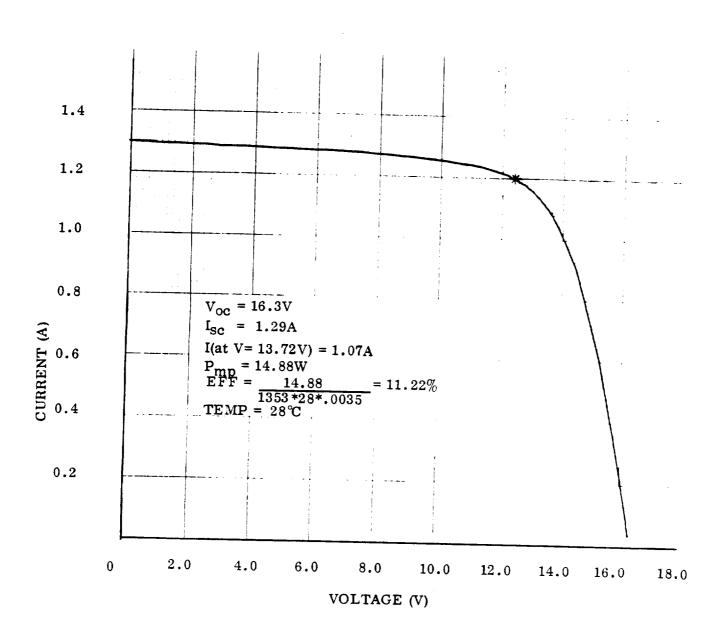


Figure 13 I-V Curve (X8517162-002)

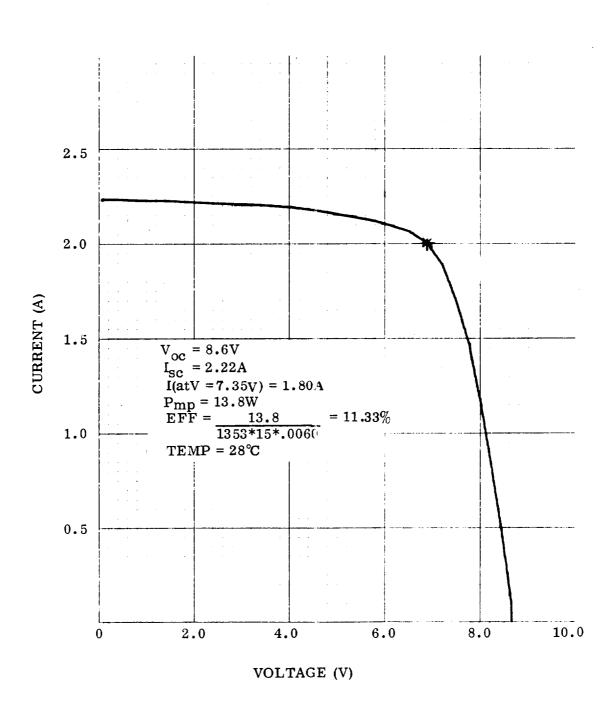
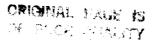


Figure 14 I-V Curve (X8517163-001)



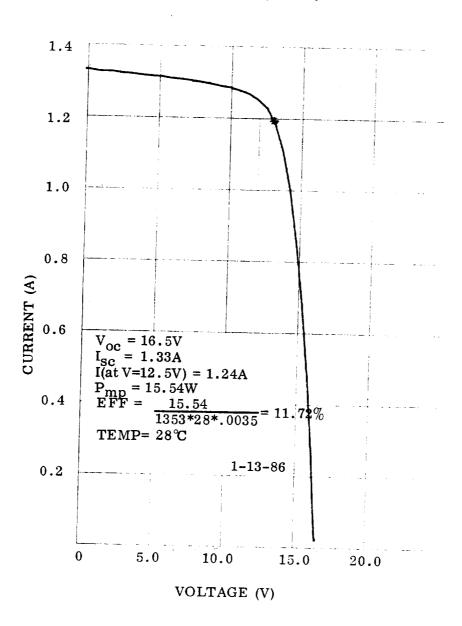
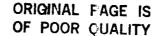


Figure 15 I-V Curve (X8512604-501)



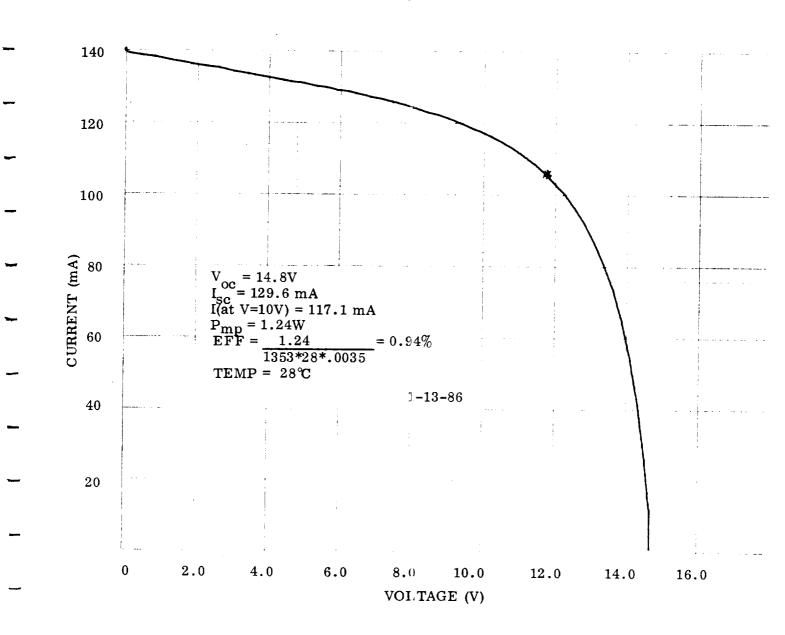


Figure 16 I-V Curve (X8512604-503)

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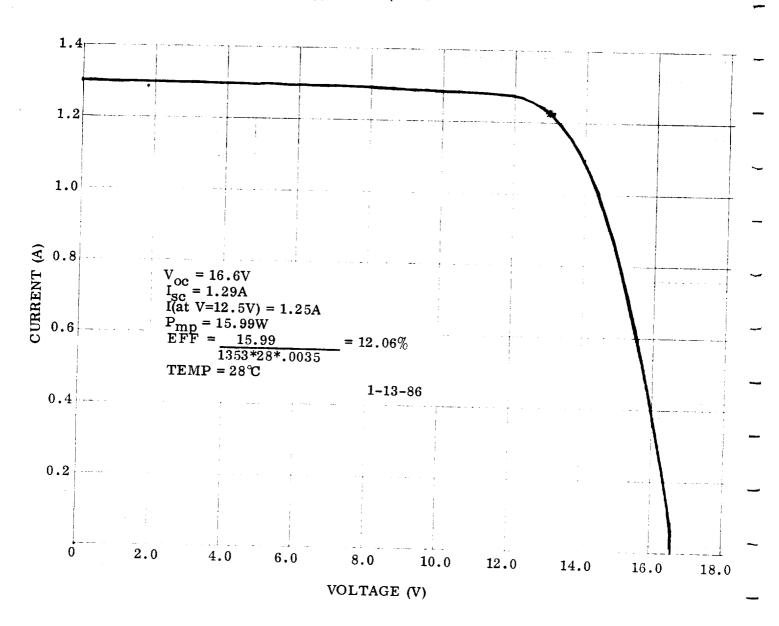


Figure 17 I-V Curve (X8517165-501)

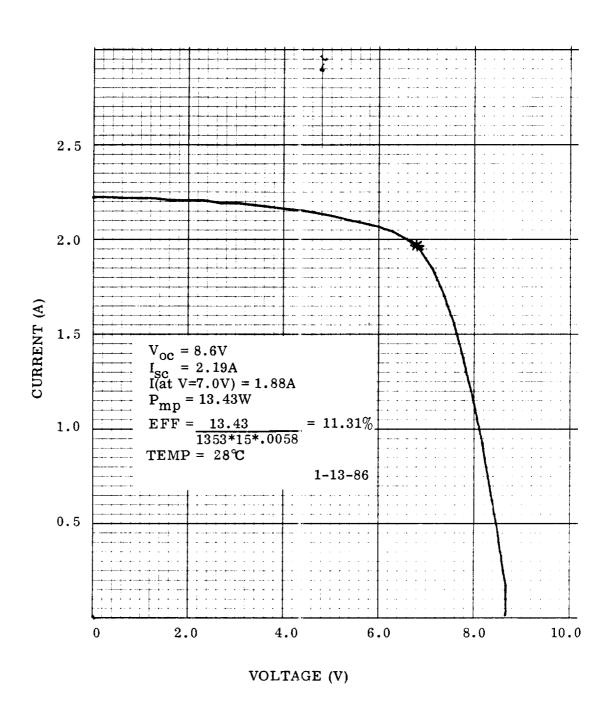


Figure 18 I-V Curve (X8517166-501)

respectively. No damage was incurred to the solar cells during adhesive bonding to the module plate.

2.4 TASK 4 - DELIVERY

The four solar cell module plates were delivered to NASA LeRC, attention Henry Curtis, on 20 January 1986. Subsequent conversation with Mr. Curtis has assured LMSC that the plates arrived safely at their destination.

3.0 FACILITIES AND EQUIPMENT

3.8

This section contains a detailed description of the facilities that would be used to support the design effort and fabrication work on Space Station flex arrays. These include areas for solar array engineering design and analysis, development, fabrication, assembly, and testing. The facilities most pertinent to the performance of this project are described in this section, which includes the following:

3.1 DESIGN AND ANALYSIS EQUIPMENT
3.2 THERMAL CYCLING EQUIPMENT
3.3 FLEXIBLE SOLAR ARRAY FABRICATION FACILITIES AND EQUIPMENT
3.4 FLASH/FUNCTIONAL TESTING
3.5 SOLAR ARRAY BLANKET ZERO-GRAVITY TESTING
3.6 FULL-SCALE MAST AND WING EXTENSION TESTING
3.7 FULL-SCALE WING ENVIRONMENTAL TESTING

SAE ASSEMBLY AND TESTING SEQUENCE

Engineering, development, and fabrication operations for LMSC spacecraft programs, for the most part, are performed at three primary sites located on the San Francisco Peninsula. The main LMSC plant is located in Sunnyvale and contains the Corporate Offices (Building 101). The Astronautics Division (AD) has offices at the main Sunnyvale plant. The Research and Development Division has offices and facilities on the second site, located near Stanford University in Palo Alto. Lockheed Research and Development Laboratory facilities have broad scientific capabilities for investigation of physical sciences. If LMSC were to perform Space Station design and fabrication work, these capabilities are available. The third major LMSC facility is the Santa Cruz Test Base (SCTB). SCTB is located in the Santa Cruz mountains west of Sunnyvale and is the location of a large antenna test range and hazardous test support facilities. It would not be utilized for Space Station work. LMSC-owned/leased facilities provide over 8 million square feet of board and desk, manufacturing, and test facilities.

LMSC has considered all of the facilities needed to support Space Station, and all facilities described herein are available for this design effort and fabrication work.

3.1 DESIGN AND ANALYSIS EQUIPMENT

The Electrical Power Systems (EPS) organization at LMSC, which will be directly responsible for solar array design, is located in Building 151. All necessary space, facilities, and support services such as the data center, reproduction, and document control are available in the immediate area to support this project. In addition, EPS has extensive computer support equipment which is listed below.

Electrical and Mechanical Design

- IBM 4361 CAD/CAM System using CADAM software
- 10 terminals within EPS area (Figure 19)
 395 terminals available throughout LMSC
- 9 electrostatic plotters linked to the CADAM system

Engineering Analysis

- EPS has 3 HP 1000 computers (Figure 20), 1 HP 9000 computer
- 20 HP 150 work stations
- Using a networking hookup, the CRAY 1R computer (Figure 21) and VAX 11/780 computer are available for EPS use (Figure 22)
- 1 VAX 11/780 computer is available for Dynamic Modeling Analysis in the LMSC Star Lab (Figure 23) in Building 104

With the CAD/CAM system, computer analysis equipment and data management support services, the EPS organization minimizes labor inducive tasks and maximizes the design and analysis efforts of its engineers. LMSC educates its employees through company training courses on how to get the most out of available equipment and software.

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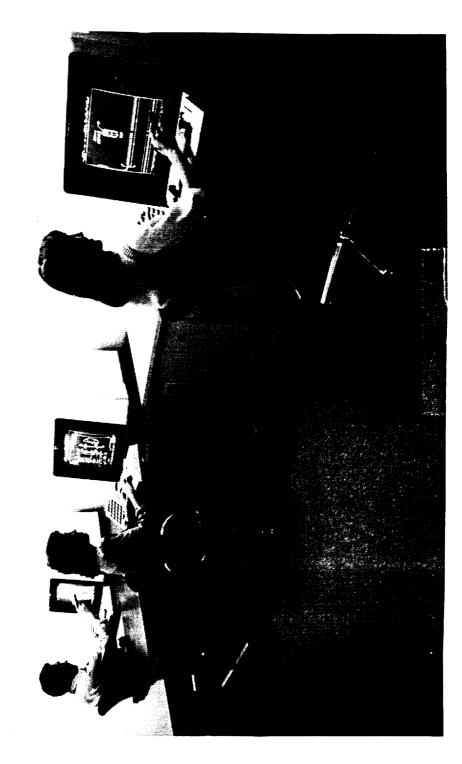


Figure 19 CADAM System Terminals



Figure 20 Electrical Power Systems H-P 1000 Terminals

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Figure 21 Cray 1R Computer

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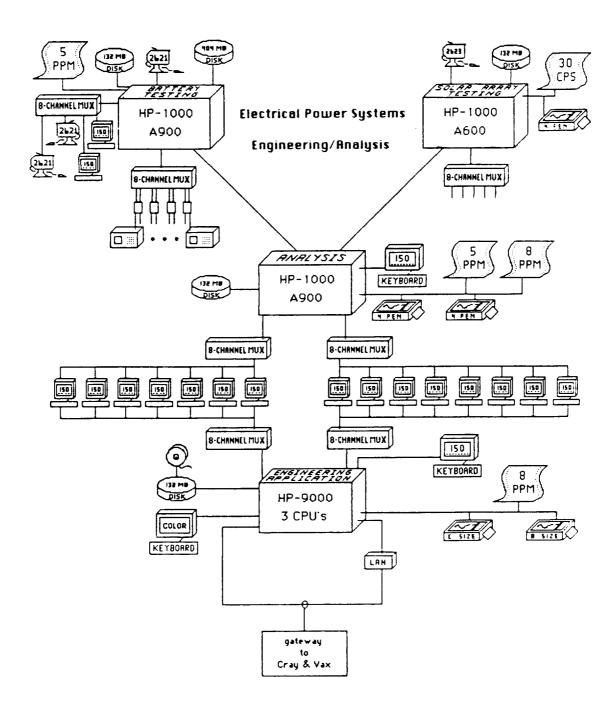


Figure 22 Electrical Power Systems Computer Network



Figure 23 Star Lab VAX II/780 Computer and Terminals

3.2 THERMAL CYCLING EQUIPMENT

The test facilities for thermal cycling are a part of the EPS Laboratory. This lab consists of approximately 5,000 square feet dedicated to power systems test and evaluation. The solar array capabilities in the lab are approximately 2,000 square feet and consist of the necessary facilities and capabilities for completing thermal cycle testing.

Solar Array Laboratory

5 Convective Thermal Cycle Chambers

These chambers are used to perform thermal life cycle testing on solar array panel and substrate assemblies to assess failure modes and determine thermal/electrical performance for a given number of thermal cycles. The EPS lab has over 100 square feet of available chamber space to perform these types of tests.

• 3 Thermal Vacuum Cycling Chambers

The solar array lab has three chambers capable of performing electrical and thermal performance tests in a 10 (-8) torr environment which can be cycled thermally from -300°F to +200°F. Additionally, each chamber has two fused quartz windows so a light source can be directed at the test samples and electrical measurements can be made at the test conditions.

• 3 Calibrated Light Sources

The solar array testing facility has three calibrated light sources available for use on test samples. Two Spectrosun X-25 solar simulators capable of >1 sun and a portable XT-10 simulator for special applications and field use.

Portable Solar Test Facility

To accommodate special test requirements the solar array lab has a portable solar cell/array test set which includes a 1 sun solar simulator and a data acquisition and control system to take and manage acquired test data.

Test Data and Control System

To manage test operations, acquire data, and perform test data analysis; the solar array lab utilizes an HP 1000/A600 minicomputer in a real time mode. This facility is capable of monitoring and controlling eight simultaneous tests with a total data acquisition capability of 500 channels. There is graphics display and hard-copy capability available in the test area.

• Laboratory Layout

The lab is arranged to provide testing to six test stations from a rotating X-25 solar simulator. This is illustrated in Figures 24 and 25. The floor plan is shown in Figure 26.

Because of its availability and accelerated cycle time, Quick Look Box III would be used to perform thermal cycle testing. This new chamber, shown in Figures 27 and 28, has multi-mode capabilities with three individually controlled sub-chambers. Each sub-chamber can take solar array specimens up to 36" x 36" or a single panel of 36" x 96" if the inside chamber walls are removed. This facility is presently in use to thermally cycle gallium arsenide solar cell strings and a panel segment of 5.9 x 5.9 cm solar cells for one of our program applications. This facility/chamber was designed and fabricated for LMSC, based on our successful thermal cycling in Quick Look Box I of the SAE 2 x 4 cm and 5.9 x 5.9 cm panel segments in support of the panel verification.

3.3 FLEXIBLE SOLAR ARRAY FABRICATION FACILITIES AND EQUIPMENT

The facilities required for the fabrication of the flexible solar array panels are in place in LMSC's new solar array fabrication facility in Building 153 (Figure 29) of the Sunnyvale plant. This area was the home of the SAE assembly and deployment testing for four years. After a \$3.2 million upgrade, Building 153 consists of a 30,000 square foot processing area for fabricating polyimide/copper solar cell interconnect circuits, and a final assembly clean room for circuit to substrate bonding, wiring, and testing. The circuit processing area consists of a series of conveyorized equipment for drilling, laminating, photo processing, copper etching, and final cleaning operations.

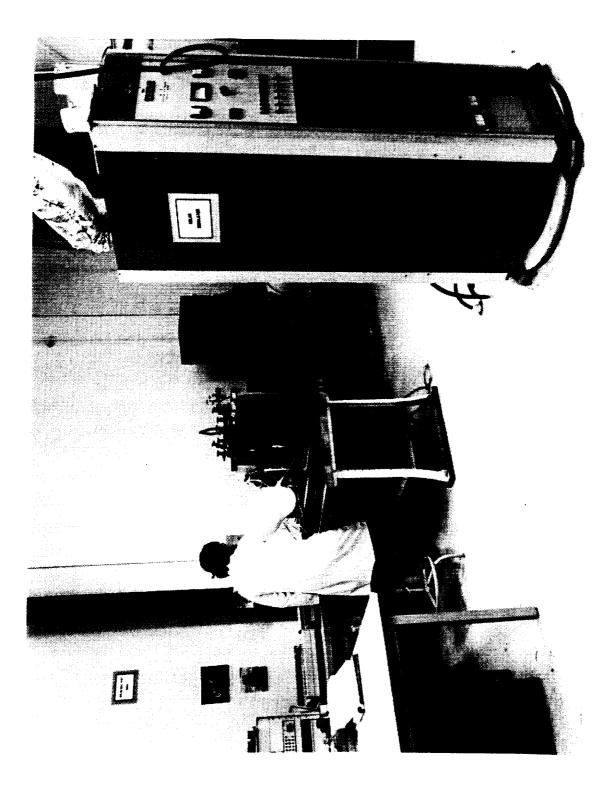


Figure 24 Solar Array Laboratory Solar Cell Testing

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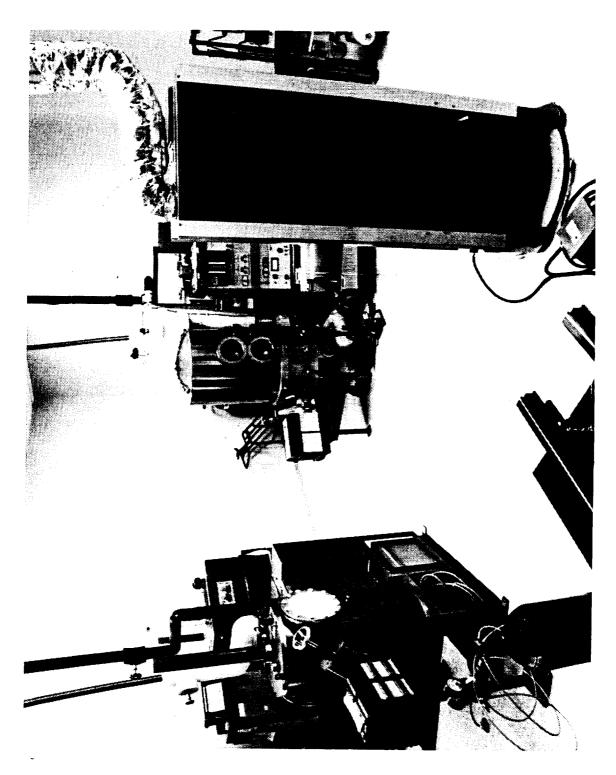


Figure 25 Solar Array Laboratory Thermal Cycling Chambers

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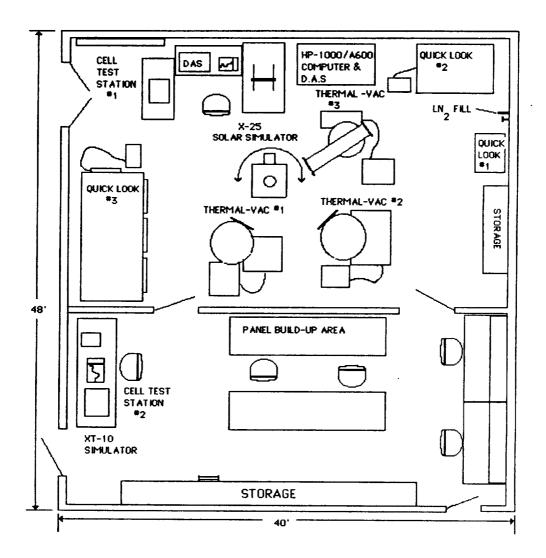


Figure 26 Solar Array Laboratory Layout

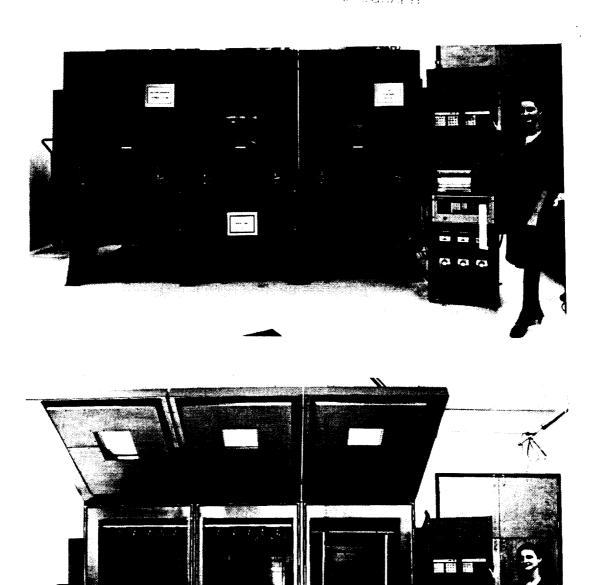


Figure 27 New "Quick Look Box III" Convective Thermal Cycling Chamber

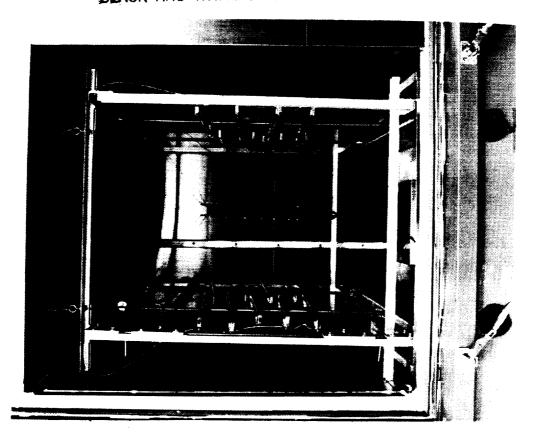
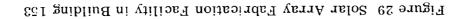
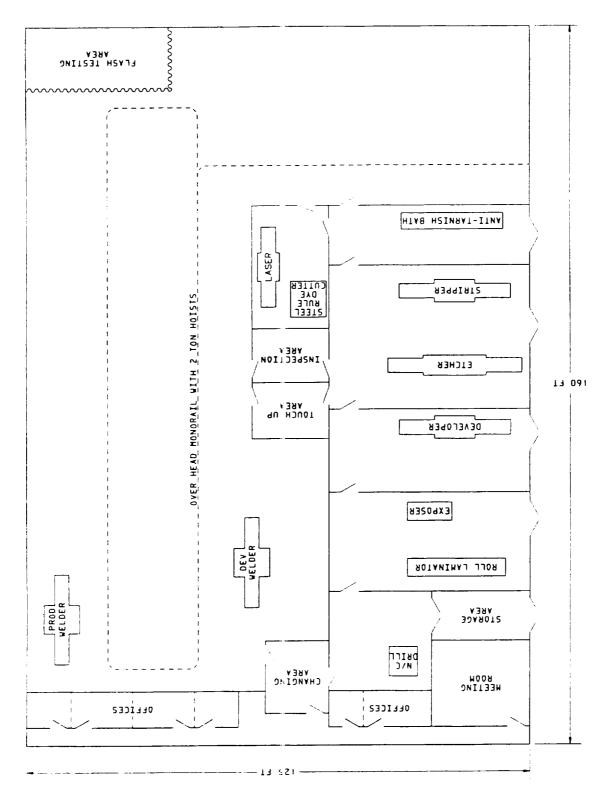




Figure 28 Quick Look Box-III - Specimen Mounted for Test





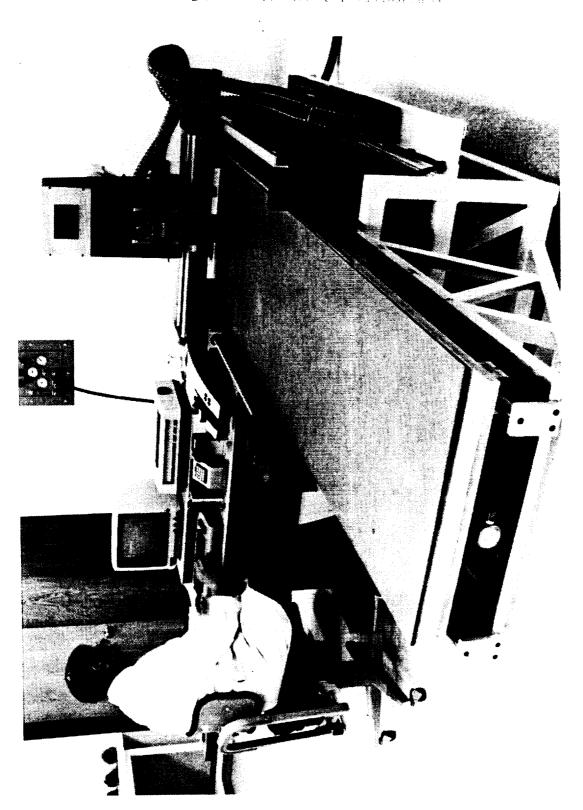
In addition to the Building 153 solar array fabrication facility, Building 151 has a solar array fabrication facility which supports existing DoD contracts that utilize conventional assembly technology consisting of discrete silver plated molybdenum interconnects soldered to 2 x 4 cm solar cells. The new Building 153A facility is scaled to handle high production assembly requirements for new DoD contracts including the MILSTAR program. The circuit process incorporates the use of a custom design N/C drill (Figure 30) for providing solar cell contact weld access holes in a one mil adhesive coated polyimide (kapton) dielectric film. This machine is capable of drilling a 20" x 80" circuit in a continuous roll set-up. Following the drilling of a quantity of circuits (up to 500 linear feet) the polyimide film is laminated to a roll of copper foil using a continuous roll lamination process. This laminator (Figure 31) is also used for laminating a dry film photo resist which is used for controlling the copper circuit configuration during etching.

Following the resist application, the circuits are processed through the photo etch processes consisting of a UV exposer (Figure 32) to establish circuit configuration, a conveyorized semi-aqueous photo resist developing station (Figure 33) and a copper etcher (Figure 34) to remove unnecessary copper from the circuit. The final circuit processes include a photo resist stripping process (Figure 35) and a final cleaning and anti-tarnish coating process (Figure 36). The completed circuit is then ready for net trim and is stored in nitrogen cabinets until ready for welding of large area wraparound contact solar cells.

The panel assembly area of this facility consists of a 18,000 square foot clean room. In this area the solar cell welding, circuit electrical checks, circuit bonding and final wiring and panel electrical checkout are performed.

The solar cell welding system is a state-of-the-art design using a Hughes parallel gap electrode tip and power supply with several process control and monitoring systems incorporated into the electronics. The primary control for the weld pulse is a Vanzetti I-R sensor that performs an in-process reading of the weld temperature and terminates weld energy when a pre-set temperature is achieved. Other monitors take readings on tip force, weld voltage, current, weld energy, tip contamination and weld duration.

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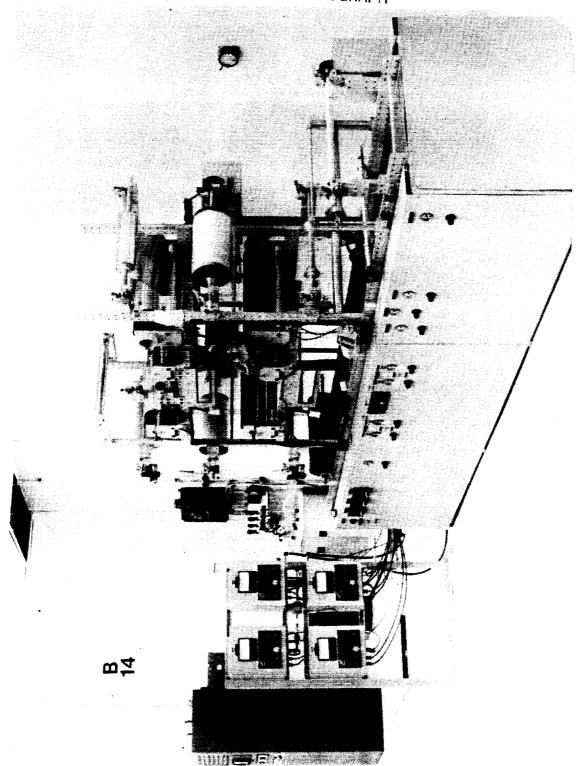


Figure 31 Flexible Circuit Roll Laminator

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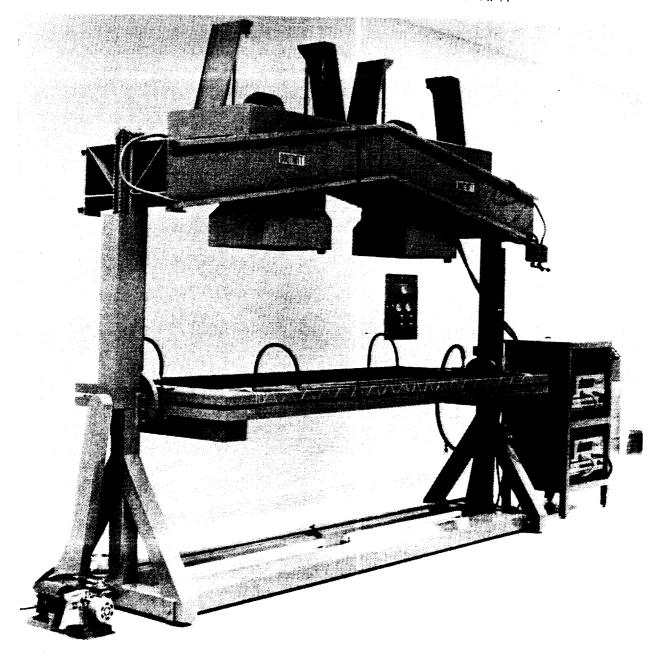


Figure 32 Flexible Circuit Photo Resist Exposer



Figure 33 Flexible Circuit Photo Resist Developer

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Figure 34 Flexible Circuit Copper Etcher

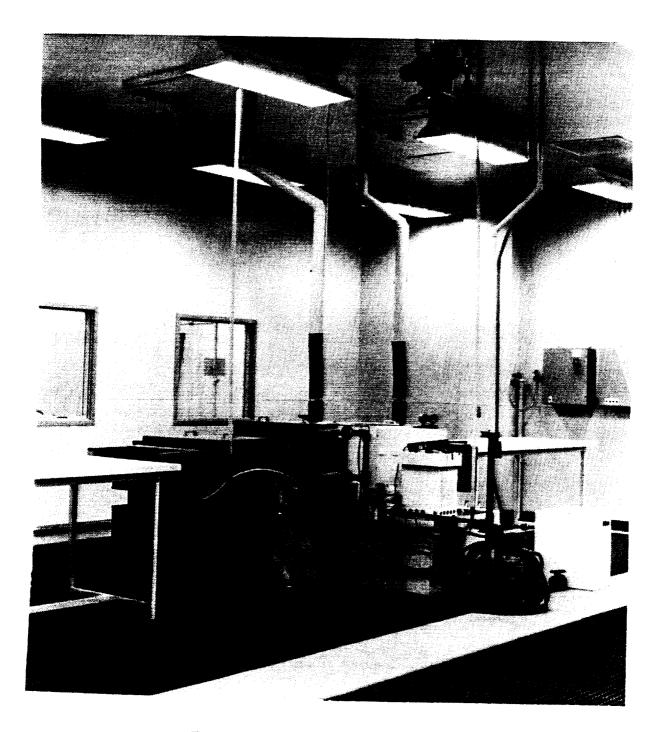


Figure 35 Flexible Circuit Photo Resist Stripper



Figure 36 Copper Anti Tarnish Coating

All of this data is stored on a hard disk for later verification of weld quality. This welder incorporates a 20" x 80" N/C controlled table movement. Two camera systems are used for controlling and monitoring the welding in process. A precision locating camera performs final alignment of the weld area under the weld tips prior to each weld. The second camera is a CCTV monitor of the welding process which is displayed on a remote screen. This can be video taped for later correlation with the hard disk data to get complete history of each weld for each circuit. Two welding systems are in place. One welder is used for production work (Figure 37) and the other welder is used for development work (Figure 38). In 1987, the development welder will be moved to the advanced manufacturing area in Building 588, and a second production welder will be installed in Building 153 to accommodate the larger scale production needs of the MILSTAR program.

All flexible solar array fabrication equipment is available in Building 153 except for autoclaves which would be needed if autoclaving of superstrates to welded submodules is required. This capability exists in the main manufacturing shops. If production needs require it, an autoclave would be dedicated to this project to accommodate schedule constraints.

3.4 FLASH/FUNCTIONAL TESTING

LMSC currently has three pulse light test systems available in our manufacturing area to provide full illumination testing of the modules and panels. The 2×4 cm and 5.9 x 5.9 cm SAE panel segments were successfully tested prior to and after the flight and ground testing. Figure 39 shows a SAE panel mounted to a pegboard for electrical testing. The new facility will have a Spectrosun pulse light source available for testing small modules and panel wing segments.

3.5 SOLAR ARRAY BLANKET ZERO-GRAVITY TESTING

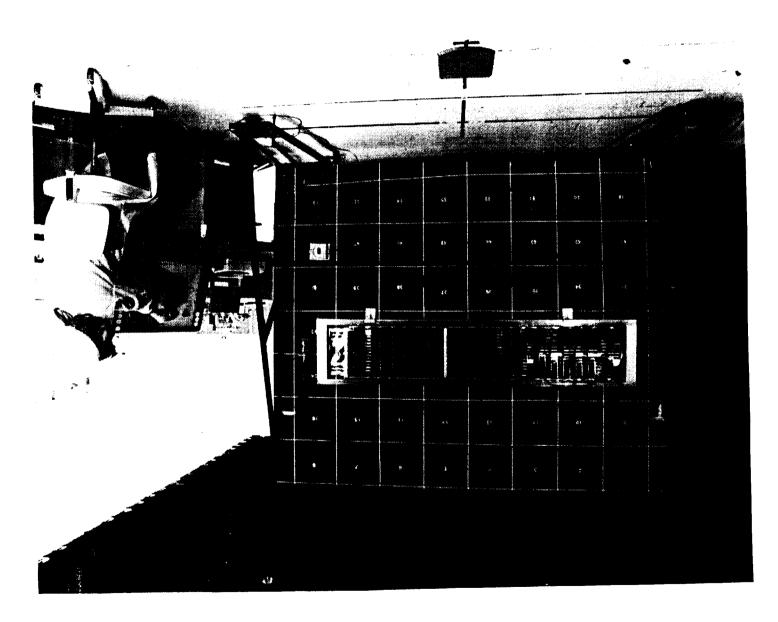
After developing an advanced solar array, a test will be required to demonstrate the retraction capability of the solar array panel segments in a zero-gravity environment. The Solar Electric Propulsion (SEP) solar array was tested by constructing a test fixture (Figure 40) and flying the experiment in a KC-135 airplane (Figure 41). By performing a parabolic flight maneuver, a simulated zero-gravity environment was



Figure 38 Flexible Circuit Development Welder

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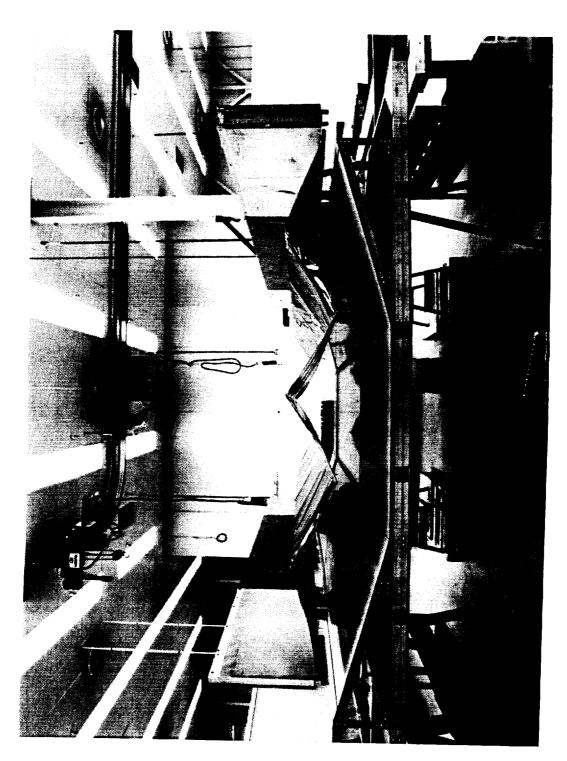
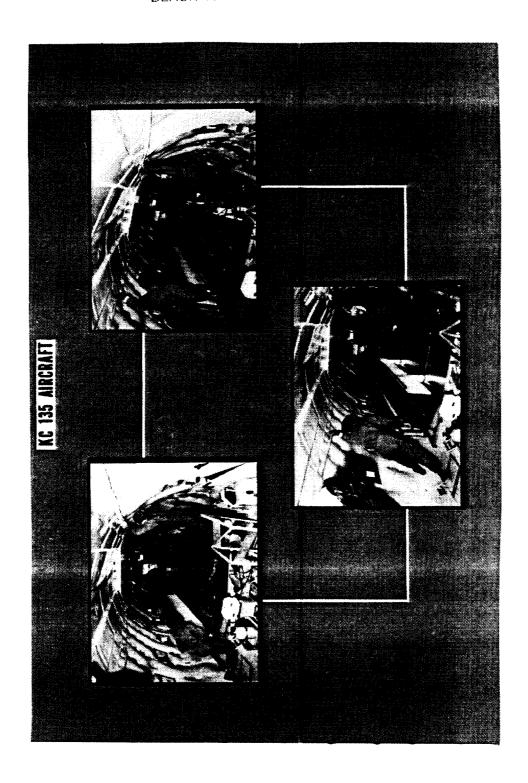


Figure 40 SEP Solar Array Zero-Gravity Experimental Setup

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obtained for approximately 30 seconds. A similar test could be done with the Space Station arrays.

With LMSC's experience performing this test, no problems can be foreseen in repeating it in the future. LMSC would use a KC-135 airplane from NASA-JSC (Ellington AFB) because of our successful teaming arrangement with them in the past. No aircraft availability problem can be foreseen.

3.6 FULL-SCALE MAST AND WING EXTENSION TESTING

In addition to solar array fabrication, the Building 153 facility would also be the location for a series of functional and acceptance tests on the mast and solar array wing. The mast would be tested first as a component, and then the whole solar array wing would be tested.

The mast tests would most likely include functional extension and retraction (both loaded and unloaded), linear and angular alignment measurements at intermediate and fully extended positions, torsional and bending stiffness measurements, flight loading, and lock-up loading tests. To simulate a zero-gravity environment, a water table (Figure 42) would be set up. Because LMSC has done this testing once before, no problems are anticipated.

The solar array wing would need to be functionally tested to demonstrate its capability to properly perform "hands-off" extension/retraction operations. To demonstrate this capability, a simulated zero-gravity test setup would be required. This test was performed once before in the Building 153 facility, see Figures 43 and 44. The monorail which was used to support the wing while being extended and retracted is still in place in the facility. Additional test support equipment would be required, but no problems in completing this task are foreseen.

3.7 FULL-SCALE WING ENVIRONMENTAL TESTING

Three environmental tests would be performed to test a full-scale wing. These tests would include vibration, acoustic noise, and thermal vacuum cycling. The test facilities required for these three tests are located in the Sunnyvale facility. These

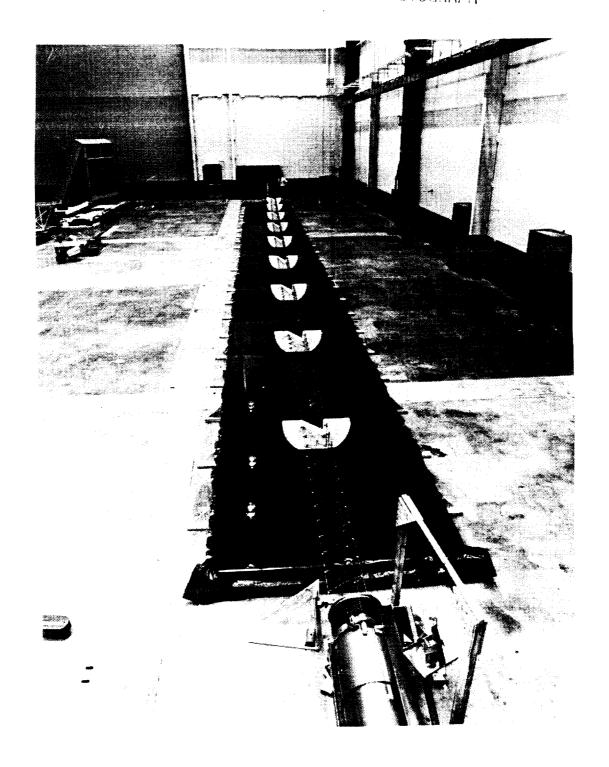


Figure 42 General Test Setup

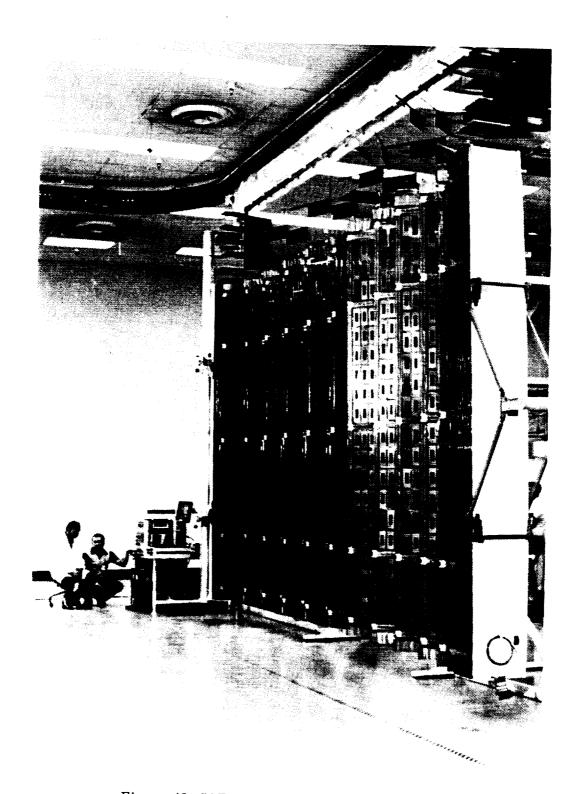


Figure 43 SAE Being Deployed in Building 153



Figure 44 SAE Fully Deployed in Building 153

facilities are the same as those used on the Solar Array Experiment (SAE). Figures 45 through 48 show the acoustic, vibration, and thermal vacuum cycling setup of the SAE and SEPS hardware. The experience gained on these previous tests would provide the basis of accurate cost and performance estimates if these same facilities were used for this project.

3.8 SAE ASSEMBLY AND TESTING SEQUENCE

The overall SAE fabrication and assembly capabilities and methods are shown in the flow sequence shown in Figure 49. Many of these same methods would be used on Space Station solar arrays if LMSC became involved in fabrication work.

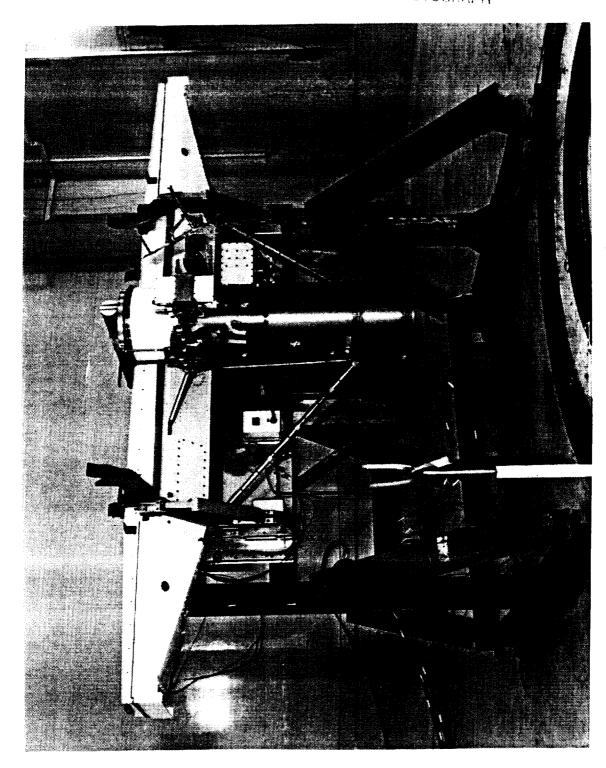


Figure 45 SAE Acoustic Noise Test - Mounted on Simulated Support Structure

DATE: FEBRUARY 1979

FACILITY: LMSC BLDG 156
ACOUSTIC CELL 2 (20 FEET
BY 26 FEET BY 31 FEET HIGH)

OBJECTIVE: SUBJECT THE STOWED WING ASSEMBLY TO A QUALIFICATION LEVEL ACOUSTIC ENVIRONMENT (145 dB OAL)

SETUP: SUSPENSION 6 FEET ABOVE CELL FLOOR ON BUNGIE CORD AND WIRE ROPES

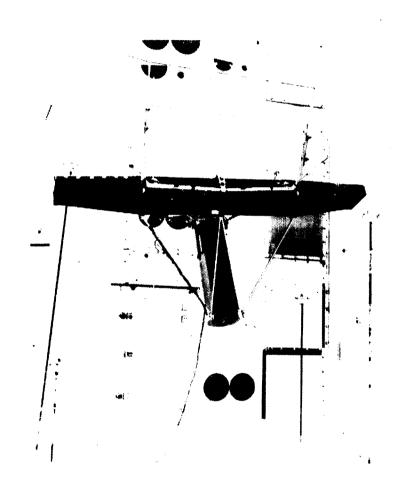


Figure 46 SAE Acoustic Noise Test - No Support Structure

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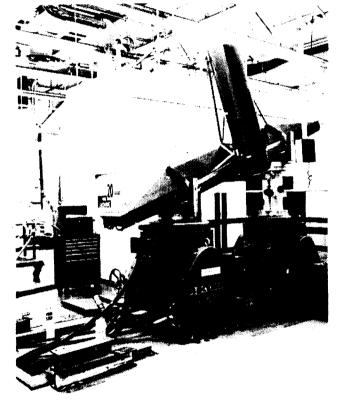
DATE: MAY 1979

FACILITY: LMSC BLDG 102 HIGH BAY AREA

OBJECTIVE: SUBJECT STOWED WING ASSEMBLY TO THE SPACE SHUTTLE DYNAMIC ENVIRONMENT

SETUP: DUAL SHAKER SYSTEM TO SIMULATE SINUSOIDAL AND RANDOM VIBRATION

Z-AXIS TEST



X Y AXIS TEST

Figure 47 SAE Vibration Test - Two Large Shaker Tables

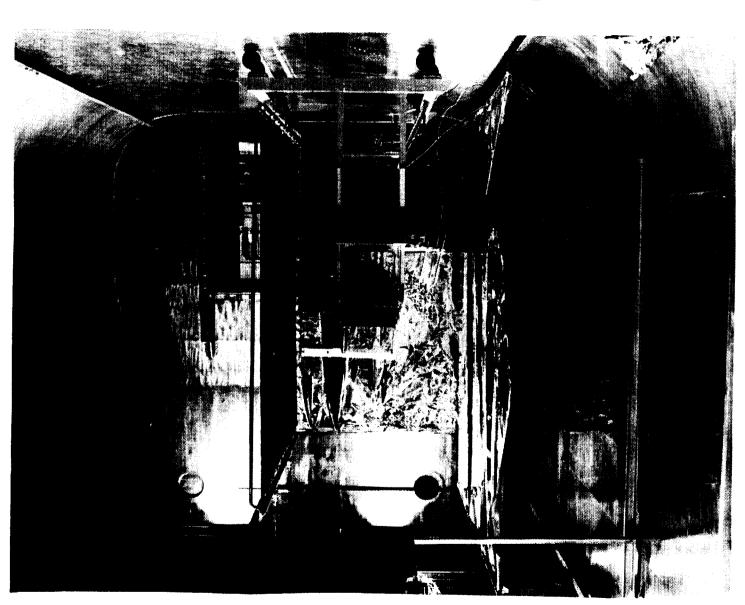
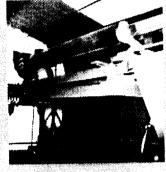


Figure 48 Full-Scale Wing Thermal-Vacuum Test Setup

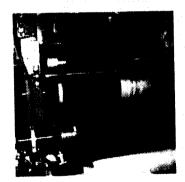
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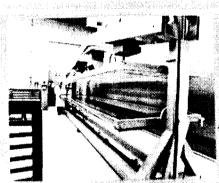
2. PNEUMATICALLY OPERATED PUNCH & DIE ASSEMBLY



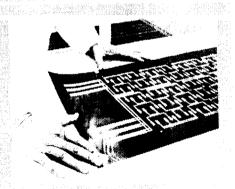
a PREPUNCHED FILM ON ROLL LAMINATOR



4. PHOTO RESIST ROLL LAMINATED ON COPPER/ POLYIMIDE LAMINATE



5. 4½ FT. × 20 FT. CONTACT PRINTER



6. NETWORK IMAGE ART MASTER

Figure 49 Fabrication, Assembly, and Test of SAE Wing

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Figure 49 Fabrication, Assembly, and Test of SAE Wing (cont.)

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Figure 49 Fabrication, Assembly, and Test of SAE Wing (cont.



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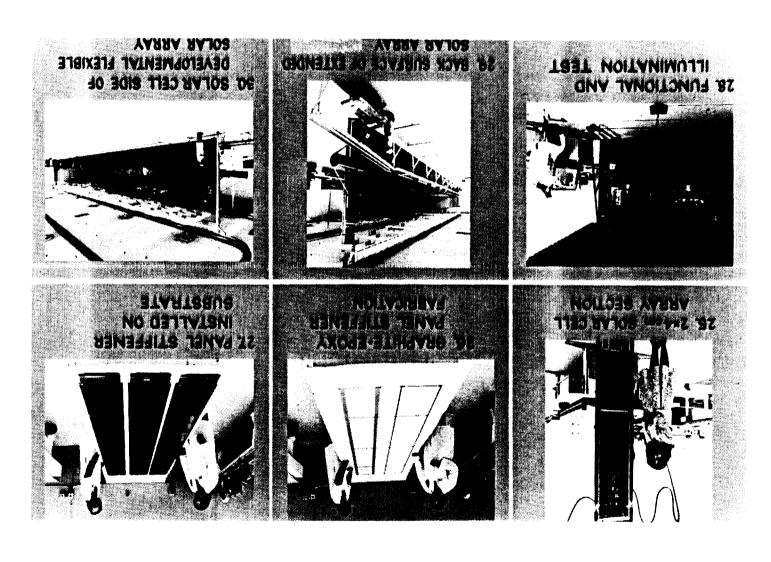


Figure 49 Fabrication, Assembly, and Test of SAE Wing (cont.)

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4.0 SUMMARY

Two modules consisting of 28 large area 5.9 cm x 5.9 cm wraparound contact solar cells welded to a flexible Kapton circuit were fabricated. In addition, a soldered conventional n-bar contact 5.9 cm x 5.9 cm-28 cell module was fabricated along with a 15 cell module utilizing 8 cm x 8 cm wrap-through contact solar cells welded to a flexible Kapton circuit. These modules contain features to allow experimental evaluation of the effects of insulation, pin-holes and other factors on several design options to gain a basic understanding of plasma interaction with solar arrays. Pretest I-V measurements were made on each module string. The module plates were delivered to NASA Lewis Research Center where they are currently undergoing plasma testing.

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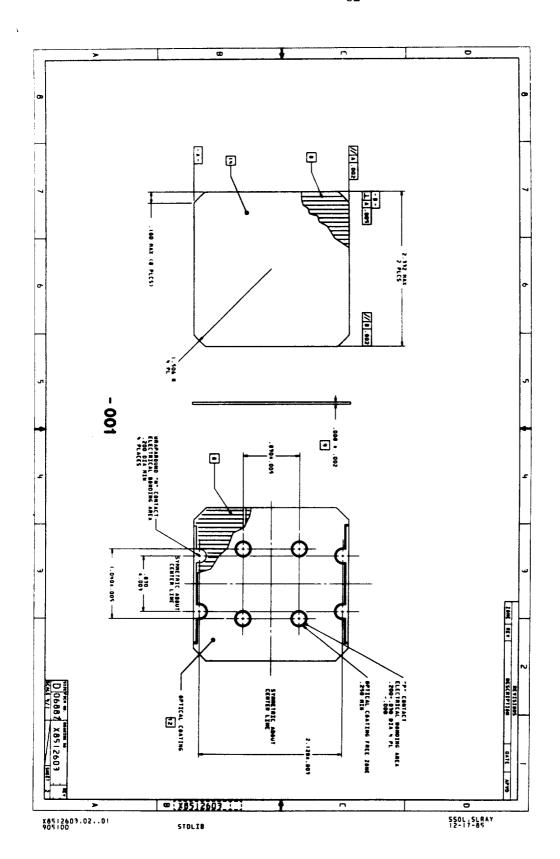
APPENDIX A

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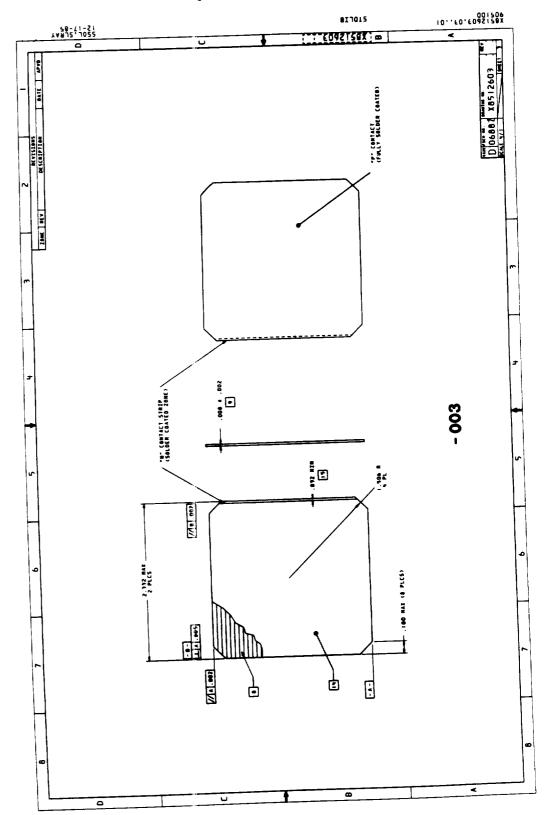
7 6 SUPPLIED BATA LOCEMEED BATA ZOME REV DESCRIPTION QUANTITY REQUIRED PER ASSERBLY (001 --SPECIFICATION **** ---APPLIED SOLAR ENERGY CORPORATION 18512403-00 SOLAR CELL 7699230 APPLIED SOLAR ENERGY CORPORATION X8512609-009 SOLAR CELL 7699230 MOTES: IT ACCEPTABLE LIMITS FOR COSMETIC DEFECTS: DOCUMENTATION AND CHANGE CONTROL REQUIREMENTS SHALL BE IN ACCORDANCE WITH THE PROCUREMENT DOCUMENT A) EDGE CHIPS ON CELLS SHALL NOT EXCEED .090 INCHES IN DEPTH BY .190 INCHES IN LENGTH. CHIPS LESS THAN .005 INCHES IN DEPTH SHALL BE DISREGARDED. 2 SPECIFICATION LISTED IN LOCKMEED DATA BLOCK ABOVE GOVERNS THE PROCUREMENT AND ACCEPTANCE OF THIS ITEM. B) CORNER CHIPS ON CELLS SHALL MOT EXCEED .000 INCHES ALONG THE HYPOTEMUSE. T PACKAGING AND PRESERVATION SHALL BE AS DETICAL COATING TO EMMANCE TRANSMISSION BETWEEN 1.1 AND 2.5 MG. 4 MAXIMUM WEIGHT: 300 GRANS PER 100 ASSEMBLIES. 13 SHIPPING CONTAINERS SHALL BE MARKED. "MON-FLIGHT ITEM. OPEN SHIPPING CONTAINERS IN CLEAN ROOM ONLY." WHEN CHANGES ARE MADE TO PROCESS SPEC-IFICATIONS CONSIDERED TO BE VENDOR PRO-PRICTARY. THE VENDOR MUST ADVISE LMSC PROCUMENT OF TWO IMPACT OF ANY CONTEN-PLATED CHANGE PRICE TO THE CHANGE AND THE SERIAL OF LOS HOWERS OF WHICH THE CHANGE WILL DREOME EFFECTIVE. AR COATING TO OPTIMIZE SOLAR CELL SHORT CIRCUIT CURRENT FOR AND OPERATOR WITH DC 97-500 AS THE ADMESTRE FOR A MICROSMEET COVERSLIDE. SOLDER COATED ZONE ON THE 'N' CONTACT STRIP SHALL EXTEND A MINIMUM OF .032 FROM THE EDGE OF THE CELL. A MAXIMUM OF .004 FROM THE CELL EDGES MAY BE FREE OF SOLDER NAMUFACTURE IN ACCORDANCE WITH PROCESS SPEC-IFICATIONS LISTED IN LOCHMED DATA BLOCK PART ABOVE ON IN SETS. AND VOLVAITION RADE BY THE VAPPHOVED VERMEN SPECIFICATIONS SHALL BE RE-PORTED IS LINSE PROCUMERRUIT. APPROVAL OF ANY DEVIATION SHALL DE FORMALLY IMPLICATED BY LINSE ISSUANCE OF A INC. ON REVISED SPECIFICATION OR ENVILOPE CHANGE PIECE A RECEPTANCE OF ANY DEVIATION CONTROL OF THE PROCUMENT OF THE PRO-PART IDENTIFICATION PER RIL-SID-17G. DO NOT HARK PARTS. PART IDENTIFICATION SMALL BE ON UNIT PART ACES AND SIMPPING CONTINUERS MINY. MO ROBE THAN NO SOLAR CELLS PER BOX. MARK LOT CODE AND CURRENT GROUP FOR EACH SOLAR CELL ON BOX. B GRID CONFIGURATION SHOWN IS FOR REFERENCE ONLY.
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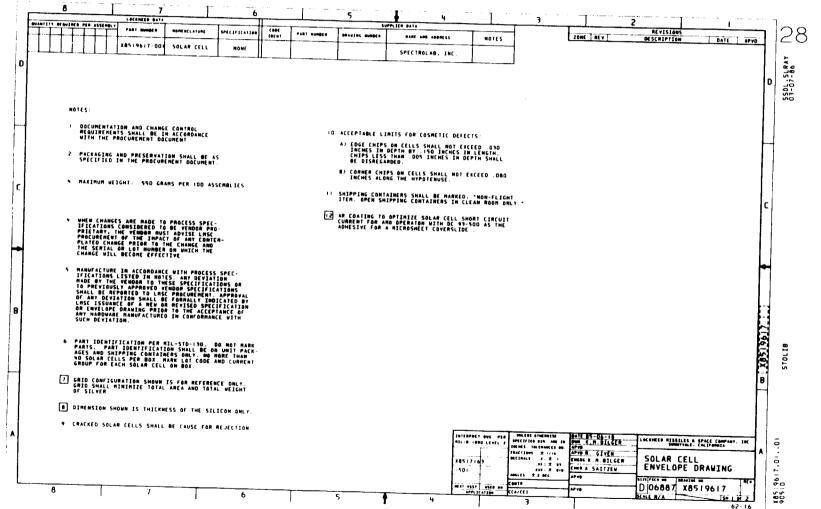
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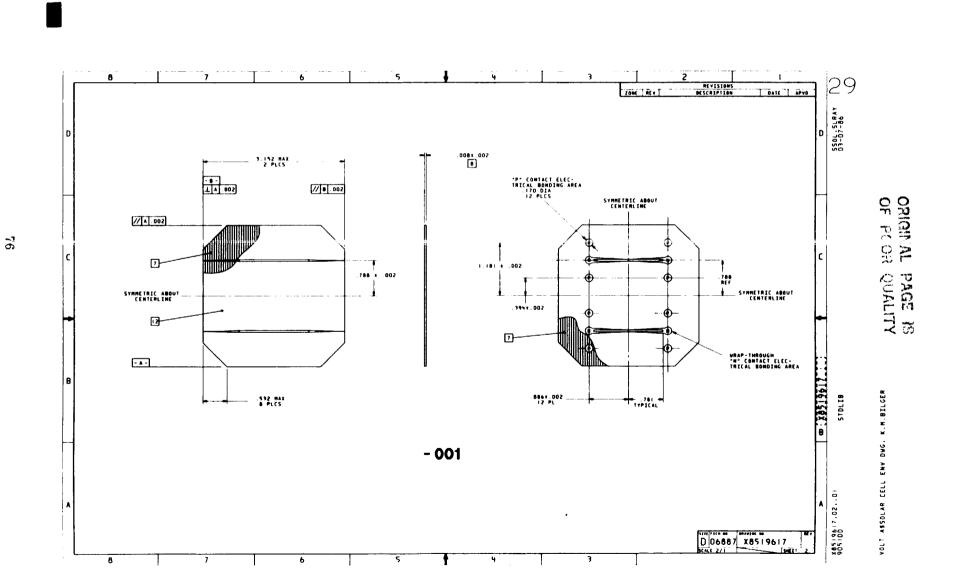


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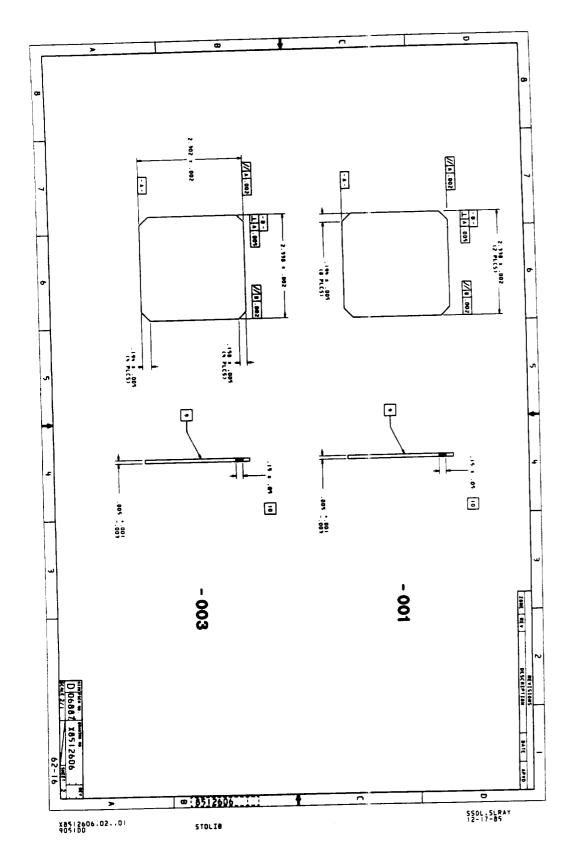




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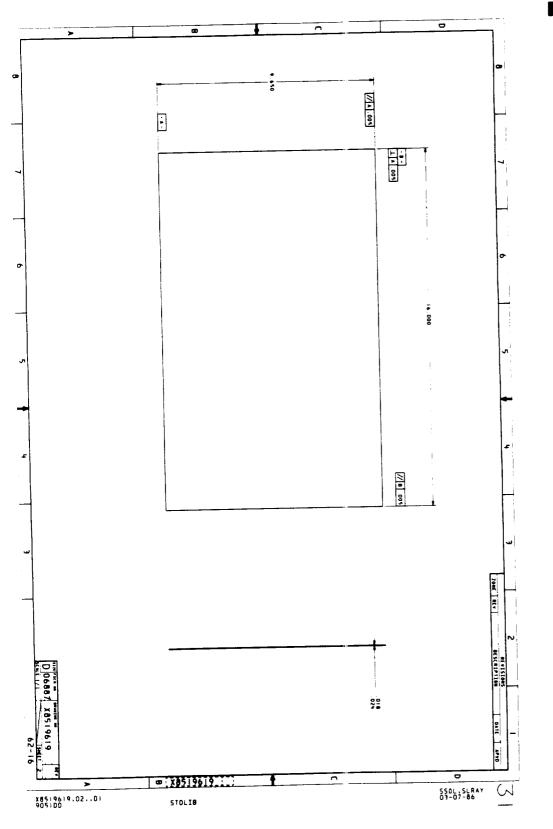
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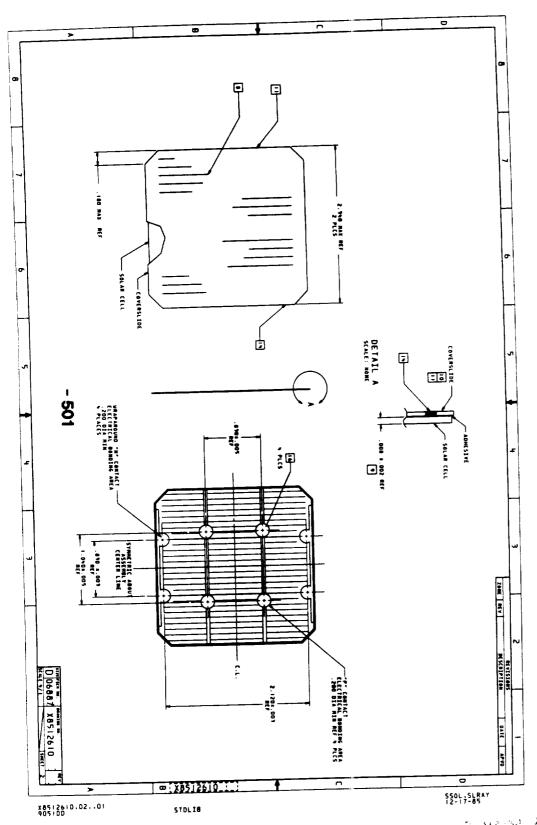
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7 6 3 LOCEMERO BATA ANAMITT REQUIRED PER ASSEMBLY PART SURGES ----SPECIFICATION 100E MEVISIONS DESCRIPTION 107 501 P481 ******* ZOME REV ---BOTES DATE APVD 1 X8512601-001 SALAR CELL 11534 APPLIED SOLAR EMERGY CORP. 5504,5LRAY 01-29-86 X8512606-00 CAVERSLIDE 7699272 PILKINGTON PERKIN FLAFO 10 X8512607-001 SOLAR CELL 8501580 11536 APPLIED SOLAR ENERGY CORP. 18512606-003 COVERSLIDE PILKINGTON PERKIN ELNEA [10] MOTES 1. DOCUMENTATION AND CHANGE CONTROL REQUIREMENTS SHALL BE IN ACCOMBANCE WITH THE PROCUMENENT DOCUMENT. 12. THE FOLLOWING DEFECTS SHALL BE CAUSE FOR REJECTION: "N" CONTACT SURFACE SHALL PROVIDE A HIMINUM SOLDERABLE A) CRACKED COVERSLIDE. WIDTH OF 0.028 TH 2. SPECIFICATION LISTED IN LOCKNEED DATA BLOCK ABOVE GOVERNS THE PROCUREMENT AND ACCEPTANCE OF THIS ITER. 8) CHACKED SOLAR CELL. COVERSLIDE SHALL OVERLAP 'N' CONTACT SOLDER BY O.OD! IN 19. ACCEPTABLE LIMITS FOR COSMETIC DEFECTS: A) ADMESTYE BUBBLES SMALL MOT EXCEED OSO INCHES IN DIAMETER ON EQUIVALENT AREA. THERE SHALL BE NO MORE THAN TEN DUBBLES PER ASSEMBLY OWNDLES SHALLER THAN ...OOS INCHES IN DIAMETER SHALL DE DISHEGARDED. 3. PACKAGING AND PRESERVATION SMALL BE AS SPECIFIED IN THE PROCUMENENT DOCUMENT 4. MAXIMUM WEIGHT: 450 GRAMS PER 100 ASSEMBLIES. 8) EDGE VAIDS OR PULL-OUT IN THE ADMESIVE SHALL NOT EXCEED .025 INCHES IN DEPIM FROM THE EDGE OF CELL OR COVERSIDE. LINGTON OF VAIR ON PULL-OUT SHALL NOT BE CONSIDERED REASON FOR REJECTION. WHEN CHANGES ARE HADE TO PROCESS SPEC-IFICATIONS CONSIDERED TO BE VERBOR PRO-PRIETARY, THE VENDOR MOST ABVISE LINC PROCURERULY OF THE LINEATY OF ARY CONTEN-PLATES CHANGE PRIOR TO VICE CHANGE PRO-INC. ISELEL OF LIT MEMBER ON MUNICAL THE CHANGE WILL DECOME EFFECTIVE. C) DELAMINATION SMALL NOT EXCEED AN AREA GREATER THAN .015 SQUARE INCHES PER ASSEMBLY. D) EDGE CHIPS ON CELLS AND COVERSLIDES SHALL NOT ERCED. 090 INCHES IN DEPTH BY 150 INCHES IN LENGTH. CHIPS LESS THAN .000 INCMES IN DEPTH SHALL DE DISREGARDED. B. MANUFACTURE IN ACCORDANCE WITH PROCESS SPEC-ILLE TONE LATTO IN LOCKINGTO DATA HE SEE VERMON TO THESE SALE PETFOLIAGE AND FOR THOSELY APPROVED VERMON SPECIFICATIONS SALES PREVIOUSLY PORTED TO LINE PROCESSION APPROVAL OF ANY DEVIAL DESCRIPTION OF THE PROPERTY OF THE SECOND DEVIAL DESCRIPTION OF THE PROPERTY OF THE SECOND CONTRACTOR SHALL DE FORMALLY IMPICATED BY LINE ENVILOPE DAMAINE PROPERTY OF THE PETFOLIAGE OF THE MARBURANT HAMPFACTURED IN COMPRIMENCE WITH SUCH DEVIAL DESCRIPTION OF THE PETFOLIAGE OF THE SECOND MARBURANT HAMPFACTURED IN COMPRIMENCE WITH SUCH E) CORNER CHIPS ON CELLS AND COVERSLIDES SMALL MOT EXCEED .000 INCHES ALONG THE MYPOTENUSE. DYRER STAIN HARK (MEF) 0135126X @ FILTERED ASSEMBLIES SHALL PROVIDE A RIBINUM ELECTRICAL CONVERSION EFFICIENCY OF 11.5E AT 1 AND 24 DEGREES CELCIUS. THE ANG CELL SHIPPING LOT EFFICIENCY SHALL BE TIBLINHOW OF 12E. ELECTRICAL 1-V CHARACTERISTICS SHALL BE INCUMED FOR EACH CELL. CELL ASSEMBLIES SHALL BE LINCUMED FOR THE PROPERTY OF THE PROPERTY ASSEMBLY AS SHIPPING CONTAINED. 7. ASSEMBLY IDENTIFICATION PER MIL-STD-130. DO NOT MARK ASSEMBLIES. ASSEMBLY IDENTIFICATION SHALL BE ON UNIT PACKAGES AND SHIPPING CONTAINERS MULY. 6 GRID COMFIGURATION SHOWN IS FOR REFERENCE ONLY AND DOES NOT MECESSARILY REPRESENT THE ACTUAL GRID CONFIGURATION. THE AREAS SHOWN SHALL BE FREE OF ARY ADMESTVE RESIDUE SUCH THAT SUBSEQUENT ASSEMBLY SOLDERING WILL NOT BE INVIBITED. DIMENSION SHOWN IS THICKNESS OF THE SILICON DNLY. TO BE FURNISHED BY LHSC. MR.655 STREBUTSE SOCCITIES DIR. AME IN INCHES. TOLERANCES ON: PRACTICOS = ± 1/16 OCCIMAÇS: .2 ± .1 .8E = ± .05 THE RY-U2-IS

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SOUTH CONTROL OF THE PROPERTY OF T 900-0-1800.LEVEL 2 COVERGLASS MUST COMPLETELY COVER THE SOLAR CELL -501 ENVELOPE DRAWING X851214 CHER A SAITZEW 12610. .2227 \$.816 MALES 2 \$ 906. APVO K. H. BILGER release no Tenantal an -501 Coute ME 27 A\$\$7 D 06887 X8512610 40 10 X851 CEALCRE 6 SCALE N/A 191 1 97 3 EJRT XXX-XXXX-XXX TRL3 62-16



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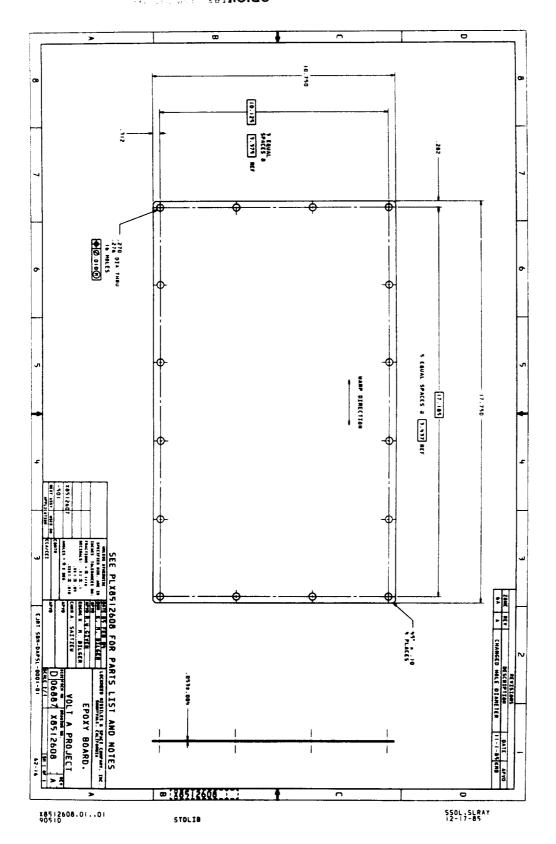
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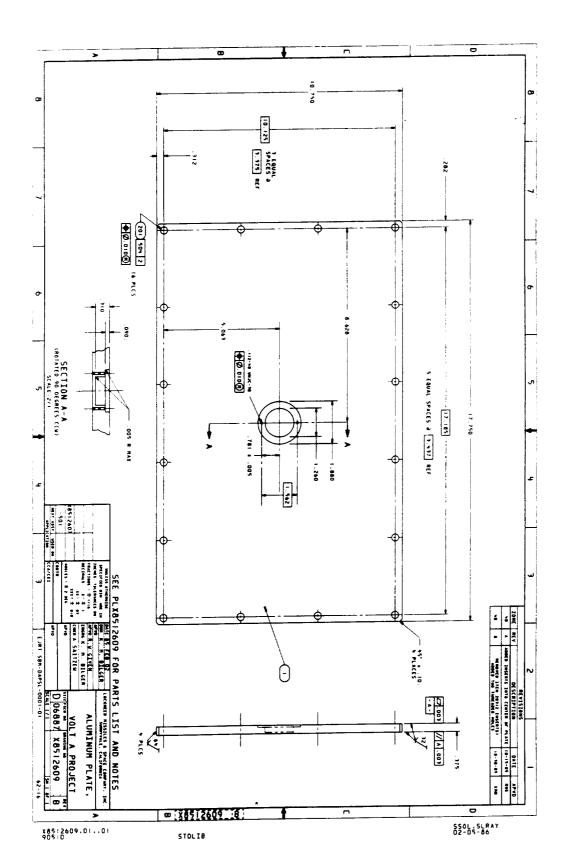
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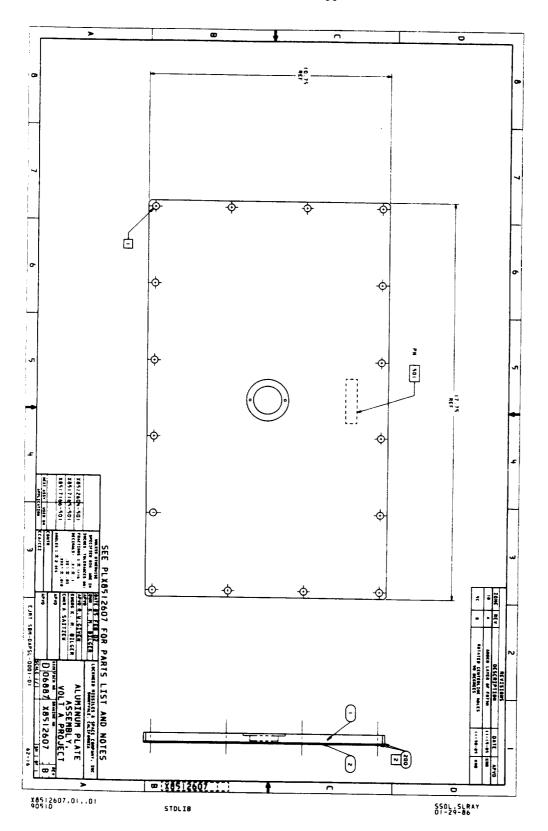
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æ ⁰⁰¹	LOCAL NOTE: US OOL WITH ITEM LOCAL NOTE: BO ITEM 201 (PRIS 1. LIGHTLY SO #400 GPIT SAND 2. SOLVENT W 4. APPLY TWO 5. VACUUM BA A. APPLY B. APPLY C. HEAT T	SE DRILL HOLES PO 002. OND ITEM 2 (EPOX MFR) AS FOLLOWS: CUFF SAND FIBERGO D PAPER. IPE ALL SURFACES LAYERS OF ADHES G AND AUTOCLAVE VACUUM OF 22 INC PPESSURE OF 20 + 0 230 +/- 10 DEG T 230 +/- 10 DEG	RIOR TO AND Y BOARD) TO LASSZEPOXY TO BE BOND IVE FILM CURE PER IT HES OF HG M Z- PSI AND REES F IN 3	DURING A ITEM 1 (BOARD LAN ED PER IT EM 504 ED INIMUM VENT VACE 30-50 MINUTE	ALUM LINATI CEM 5 CCEPT JUM JTES	IVE (IT INUM PL E (ITEM 03 USIN AS FOL	EM 200 .ATE) U 1 002) NG ACET LOWS:	O) CURING USING ITE ON SURFA	G TO EM 20 ACE T		ORIGINAL PAGE IS OF POOR QUALITY

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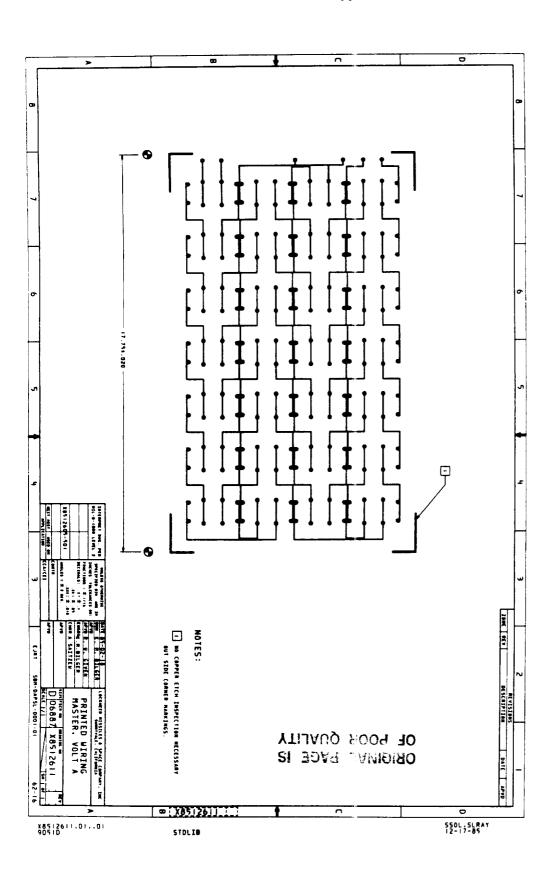
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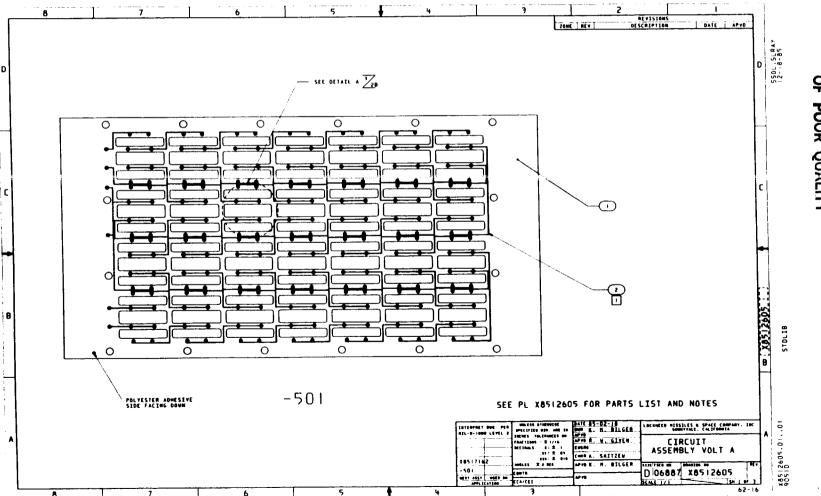
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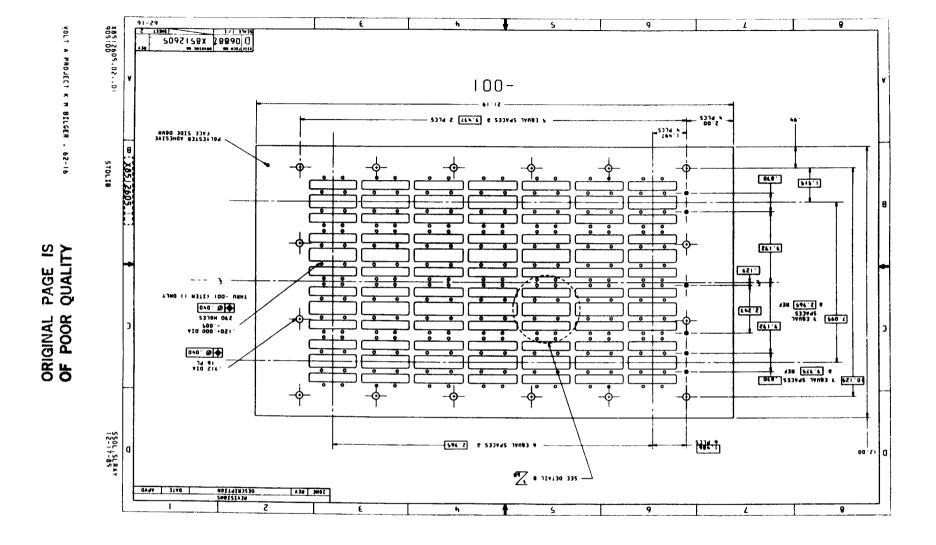


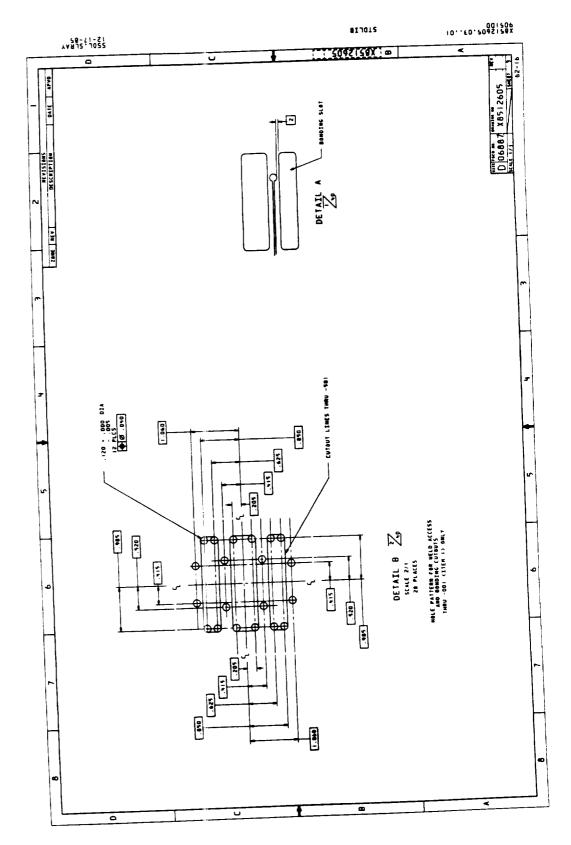
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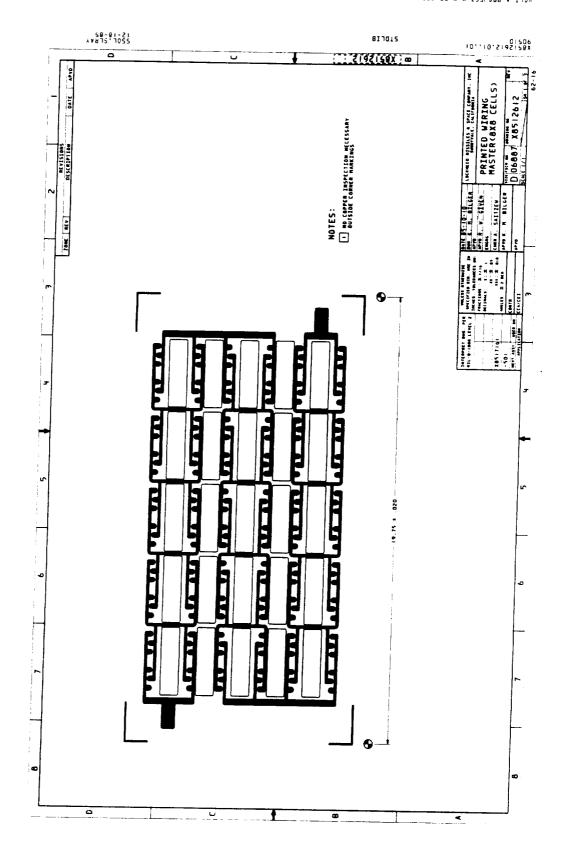


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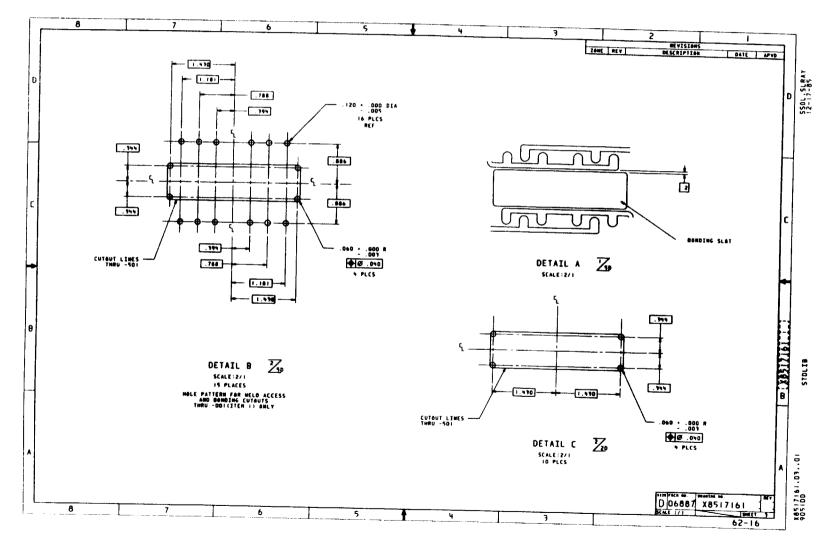
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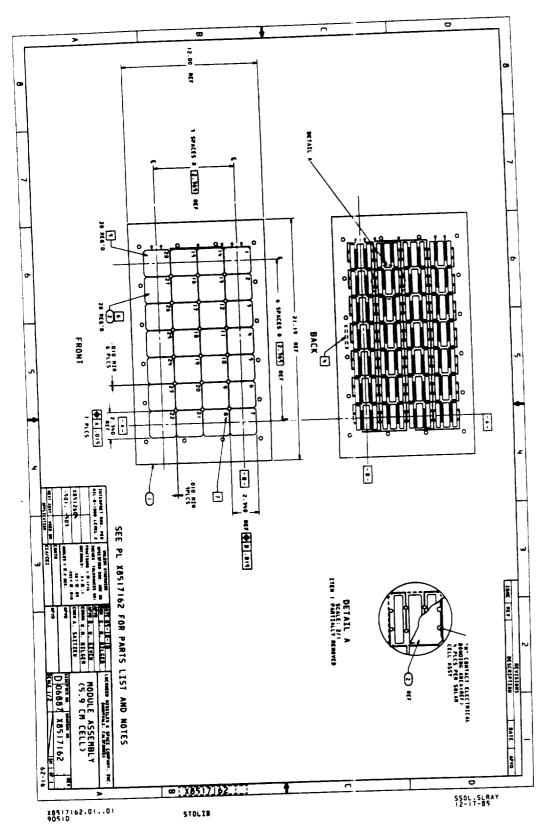
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	DO NOT MIX CUR FQUIPMENT ENGI EACH SOLAR CEL 1. NO CRACKEO 2. NO MORE TH 3. ALL SOLAR 4. COVERSLIDE	MODULE ASSY SELECT S RENT GROUPS WITHIN S	ACH CELL MODULE SHALL MEET THE AMINED WITH NOR RSLIDES. TELY COVERED BY DING ADHESIVE 4	FOLL MAL A C UBBL	Y UNLES DWING C DR CURR OVERSLI ES, EDG	S APPROVED BY RITERIA PRIOR ECTED TO NORM DE. E VOIDS, AND	THE RE	SPONSIBLE STING. SON. JT SHALL BE NO	ORIGINAL OF POOR
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VOLT A PROJECT K M BILGER . 62-16

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ND. 001	NOTE FOR CELL MO GROUPS WITH EACH SOLAR	DOULE ASSY IIN EACH CE CELL (ITEN	21 SHA	II WEET	THE SOLLE	BY THE R	ESPONSIBLE	EQUIPME	DO NOT MIX CURRE ENT ENGINEER (REE	
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ND. 001	NOTE FOR CELL MO GROUPS WITH EACH SOLAR NO CRACKED	DDULE ASSY IIN EACH CE CELL (ITEM SOLAR CELL	2) SHAI S WHEN	LL MEET EXAMINED	THE FOLLOWING CO	BY THE R RITERIA P CORRECTE	ESPONSIBLE RIOR TO TE	EQUIPME STING:		
ND. 001	NOTE FOR CELL MO GROUPS WITH EACH SOLAR NO CRACKED PRIOR TO EL	DDULE ASSY IIN EACH CE CELL (ITEM SULAR CELL ECTRICAL T	2) SHAI S WHEN I	LL MEET EXAMINED	THE FOLLOWING CAN WITH NORMAL OR RESTRATE (ITEM 3)	BY THE R RITERIA P CORRECTE PER ITEM	ESPONSIBLE RIOR TO TE: D TO NORMAI	EQUIPME STING: L VISION	N•	
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1 •	WELDING INSPE								
	OF THEIR STRE			ay THE IR	STRESS QUANT	IZER SHALL NOT	BE US	ED IN DEVEL	LOPING
2.	JOINING PROCE	DURES OR	AS A BASIS	FOR ACCEPT	ING/REJECTING	CELL WELD JOI	NTS.		
	CAL NOTE: NUME	DICAL DE	STGNATIONS F	EDR SOLAR C	ELLS ARE FOR I	POSITIONAL REF	ERENCE	UNLY AND	SHALL
007 L00	CAL NOTE: NUME T APPEAR ON PAR	RICAL DES	310114110110						
			/ TEM :	21 TO WELLE	n cell Module	USING ADHESIV	E (ITE	м 200).	
008 LO	CAL NOTE: BOND	SUPERST							
			T CVMMETDIC	AL RETWEEN	MOUNTING HOLE	S (BOTH DIRECT	IONS)	WITHIN .03	O TUTAL.
		ATE ITEM	3 SYMMETRIC	AL BETWEEN	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT Wn.	IONS)	within .03	O TOTAL.
		ATE ITEM	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN.	IONS)	within .03	O TUTAL.
		ATE ITEM COMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN•	IONS)	WITHIN .03	O TUTAL.
009 L00		ATE ITEM COMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN•	IONS)		
009 L00		ATE ITEM COMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN•	IONS)		
		ATE ITEM COMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN•	IONS)		
009 L00		ATE ITEM COMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN•	IONS)	OF POOR	ORIGNAL
009 L00		ATE ITEM	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT WN•	IONS)	OF POOR	ORIGNAL
009 L00		ATE ITEM	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	S (BOTH DIRECT	IONS)	OF POOR	ORIGNAL
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009 L00		ATE ITEM	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	***		OF POOR	ORIGNAL
009 L00	CAL NOTE: LOCAL VERGLASS MUST (ATE ITEM	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	₩. N •		OF POOR	ORIGNAL
009 L00	CAL NOTE: LOCAL VERGLASS MUST (ATE ITEM	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	***		OF POOR	ORIGNAL
009 L00	CAL NOTE: LOCAL VERGLASS MUST (ATE ITEM COMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	***		OF POOR	ORIGNAL
009 L00	CAL NOTE: LOCAL NO	OMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEEN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	***		OF POOR	ORIGNAL
009 L00	CAL NOTE: LOCAL NO	OMPLETEL	Y COVER THE	AL BETWEFN SOLAR CELL	MOUNTING HOLE EDGES AS SHO	***		OF POOR	ORIGNAL
009 L00	CAL NOTE: LOCAL NO	OMPLETEL	3 SYMMETRIC Y COVER THE	AL BETWEFN SOLAR CELL	EDGES AS SHO	APPROVAL		OF POOR	ORIGINAL PACE
009 CO	CAL NOTE: LOCAL NO	OMPLETEL	Y COVER THE	AL BETWEFN SOLAR CELL	EDGES AS SHO			OF POOR	ORIGINAL PACE :

DATE APVO

D 06887 X8517163

550L, 5LRAY 03-06-86 "N" CONTACT ELECTRICAL BOMDING AREA(REF) 4 PLCS PER SOLAR CELL ASSY DETAIL A ---2 REF • 4 BACK DETAIL A SCALE: 2/1 TTEN I PARTIALLY REMOVED 4 SPACES & 3.180 REF **-**OII 7,150 BEF **40**.015 12.00 REF 2 SPACES & 3.180 REF @ X6517163 - -7 .010 MIN 2 PLCS 15 REQ D - A -SEE PL X8517167 FOR PARTS LIST AND NOTES 3.150 a **★**A.015 | Martin Charleson | Martin St. OIPLES + 10..10.Fal7169 5 PLCS MODULE ASSEMBLY (8 X 8 CM CELL) FRONT X8517186

-501

- A -

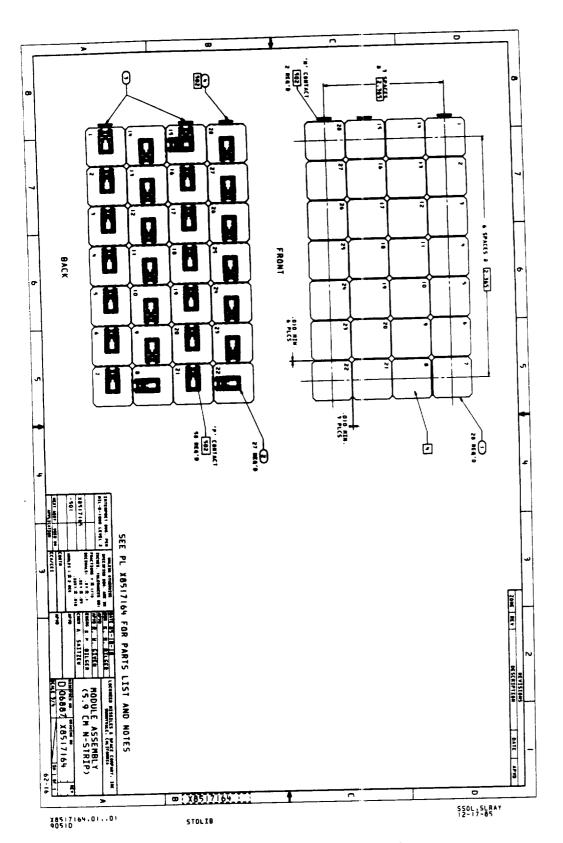
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TITLE MODULE CONTRACTO	E ASSY (5.9CM N-	STRIP)		pesign orgn _i date 6216 35 FSCMNO	DE C		OF CFE	Cui		.8517164 NEERING PART	FEV -
NAS3	24657	N11-CL11	1-0001-0	1X 96887				l 1	VOII V	ALLINIO I AINT	
TITEM I	OUANTITY PER	ASSEMBLY UNION OF MEA	NO PSCM	PART/DOCUMENT NUMBER	SEQ. NO	CCA/CI NO. IDENT	DE	SCRIPTION	ıc	C REFERENCE DESIGNATION MATERIAL/NOTES	NOTITE NO
001 002 003 004 200 400 401 500 501 502	23 27 2 1 A 2 X X X X		09474	X8512610-503 3501491-001 8501493-001 3501495-001 ACSREAGENTGRA E 1421331 7699230 LAC3575-01999 LAC3154-01001 LAC3252-01000 LAC1002-02000	3 0 0		SOLAR CELL I CELL I CELL I 2 PRUP STU PR SOLAR MARKIN SOLAR RES SOL	NTERCO NTERCO NTERCO ANOL ACTICE CELL S G METH PANEL LOERIN	NN NN NN S PEC DD	DWG PRACESTD DE MARK PER SOLDER PER PRUTECT PER	F
106 002	NOTE TED FOR FACH CELL M DO NOT MIX CURE EQUIPMENT ENGINE FACH SOLAR CELT 1. NO CRACKED 2. NO MORE TH 3. ALL SOLAR (4. COVERSLIDE	MODULE ASSY SERENT GROUPS WILLIAMSSEMBLY (IT SOLAR CELLS WAN FIVE CRACKE CELLS MUST BE DELAMINATION;	THIN EAC EM 1) SH HEN EXAM D COVERS COMPLETE INCLUDI INCHES T	ALL MEET THE TINED WITH NOR LIDES. LY COVERED BY NG ADHESIVE P OTAL PER SOLA	FOLLE MAL (A CE UBBLE R CE	WING CORR DVERSLIES, EDG LL ASSY	S APPRO RITERIA ECTED T DE. E VOIDS	PRIOR O NORM	THE TO TO TAL VI	RESPONSIBLE ESTING.	OF POOR CLASSIFY
	LOCAL NOTE: TO SHALL MEET REQU	ST CELL MODUL DIREMENTS OF I DENTIFY CELL	E ASSY I TEM 401. MODULE A	N A SUN CALIF RECOPD CURR	RATE!	D ARTIF	ICAL LI AT 13.7	GHT SC 2 V)LT	URCE .	• THE LIGHT SOUR 0 25 DEGREES C 5 TO BE •1 INCHES	

DATE APPROVAL DATE APPROVAL APPROVAL DATE DATE APPROVAL 512 F-10 ABBREVIATIONS LC = LIFE CODE SEQ NO = SEQUENCE NUMBER ORGN = ORGANIZATION

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(100 & 10P PER A MUST LYCHED 3.0 MUST LYCHED 3.0 MUST LYCHED 3.0 DOS AFTER MODULE ASSET UNDER CHE WENDOVED USING BY VILUME ANHYDA	SCO EXCEPT SULDER UP ATION, PERFORM PULL (ENDOW). NHIAB PULL LUS VHEN PULLED AT A	TOSTS ON IMENTY TOST FUSULTS MUS 0-20 DES ANGLE. THE BACK (SILVER OR ANY EVIDENCE ON TIPPED APPLICAT	REPRESENTAT ST EXCEED 5.0 SIDE OF EARTH SOLDER FLO OR SLIGHTLY	IVE SOLDER J. D LBS SHEAR ACH CELL SHAI JX. ANY SOL WETTED WITH	DINTS PER CELL V AND P-CONFRACT A LL SE VISUALLY DER FLUX RESIDUE	ENDOR REAS SHALL
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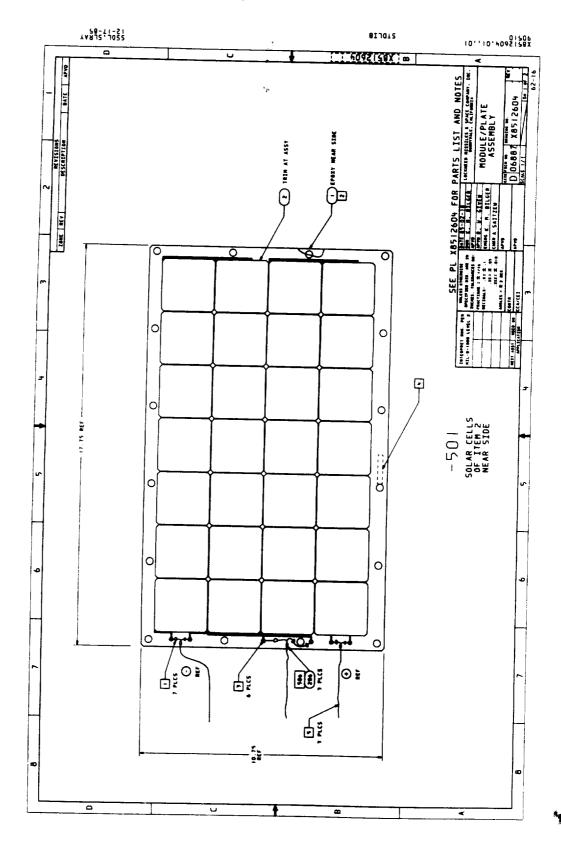
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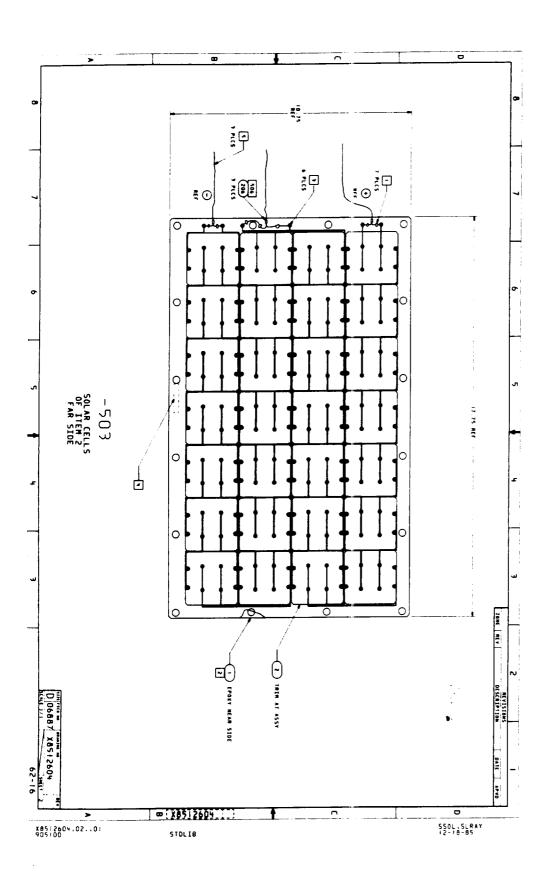
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MODULE / PLATE ASSY CONTRACT NUMBER TAILTHORITY	6216 86 MA	R 07		L x8512604	1
WAG - 6115		VCI NO.	ENC		<u> </u>
VARIOUS SUM-DAPSL-0001-01	06887		ENG	INEERING PARTS	LIST
LOCATION QUANTITY PER ASSEMBLY	PART/DOCUMENT				
TEM NO SH ZONE SO 1 503 UNIT OF NO.	NUMBER SE		DESCRIPTION	LC REFERENCE DESIGNATION/ MATERIAL/NOTES	NOTE ITEM NO.
001 1 1					
002	512607-501		AL PLATE ASSY		
200 40 40	517162-501		MODULE ASSY	5.9CM CELL	
LAC	30-4639-		ADHESIVE, EPOXY		
203 AR AR	-				
204	REAGGPDE		2 PROPANOL		
205 AR AR 77 7	920-22-4		WIRE ELEC		
205 AR AR TIZE 81348 QQS 206 3 3 TIZE 80205 NAS			SOLDER	SN63 WRMAP 2 OR 3	
400 X X QX 80205 NAS			SPLICE		
500 ~ OP	21331		STD PRACTICES	DWG PRACESTD DEF	
	3851-010100		GEN ELEC SOLDER	SOLDER PER	и03
	3041-020000 3210-010000		BOND FLEX MOD		N02
503 x x ≥Ω LAC	3154-010000		FIL & ADH BOND		N01
504 X X 5"	3211-020501		SOLAR PANEL		N07
505 X X \ 7 \(\sqrt{0} \)	3575-020501		COATING SPEC	CDAT PER	N09
506	0039-69		MARKING METHOD	MARK PER	N04
	0039-09		DESIGN STD	INSTL PER	
NOTE					
5 NO. NOTE TEXT					STD
QK NOTE LINE INDICATORS (A. R. C. STC.) AS					NOTE
QK NOTE LINE INDICATORS (A, B, C, ETC.) AR	E NO LUNGER RE	EQUIRED A	ND HAVE BEEN REI	MOVED	
001 LOCAL NOTE: FILLET WIRES (ITEM 204) TO 1. SOLVENT CLEAN SURFACES PRE-CLEANED Q-TIPS AND 2. APPLY ITEM 200 IN A CO 3. CURE 48 HRS MINIMUM AT AT 75 +/- 10 DEGREES F	AIR DRY 10 MI NTROLLED MANNE 75 +/- 10 DEG	NUTES MI R.	NIMUM.	ANOL) USING	
002 LOCAL NOTE: BOND ITEM 002 TO ITEM 001 DIELECTRIC SURFACE OF ITEM 001 (AL PLAT) THAT THE FOLLOWING REQUIREMENTS ARE MET (NOTE CONTINUED NEXT PAGE)) PER IT	EM 501. APPLY AD TH	ADHESIVE TO PRIMED HICHNESS SUCH	
REPARED BY DATE LAPPROVAL		IDATE	APPROVAL	DATE	
MECKED BY BUGGET 86-03-07				DATE	
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SH ZONE	M	AEAS	L				
NOTE NOTE	TEXT						
(CUNTINUED)		E 28 SOLAR CELL	C SHALL BE B	ONDED TO TH	SUBSTRATE	THROUGH 3	BONDING
• •							
	SEUTS. 2. THE MINIMU	M BONDING AREA	SHALL BE 90%	OF THE SLO	T AREA FOR	ALL SLUIS.	
	3. BONDLINE T	HICHNESS SHALL ADHESIVE SHALL	BE .005 IN T	HICK. N. Mode Than	ONE PLACE	BETWEEN ANY	Y 2
	4. THE CURED	ADHESIVE SHALL	MAI QKINGE I	N MORE TOAT	_		
	ADJACENT S					205	
003 LOCAL NOTE	. SOLDER CIRCUIT	r WIRES ITEM 20	4 TO ITEM 2 P	ER ITEM 500	USING TIES	205•	
003 FOCKE NOTE							
004 LOCAL NOTE	: MARK PART NO.	PER ITEM 505 A	PAROX NO SINGE				or ADDROY
	. COLICE TERMINA	AL LEADS TOGETH	ER USING ITEM	1 206. SING	LE LEADS SI	HOWN SHOULD	BE APPROX
005 LOCAL NOTE 3 FT. LONG							
		OF CHECKED	SOD THE FOLL	OWING DEFE	TS BEFORE	TESTING:	
006 EACH SOLAR	CELL ASSEMBLY SINATION SHALL NOT	HALL BE CHECKED EXCEED AN AREA	GREATER THAI	.015 INCH	PER CELL A	SSEMBLY.	
	NATION SHALL NUT D SILICON AS A R	ESULT OF CRACKE	D OR CHIPPED	COVERSLIDES	S •		
1. DELAMI						OVAL SHALL	BE REQUIRED
1. DELAMI 2. EXPOSE			-ecete cuali				
1. DELAMI 2. EXPOSE 3. CRACKE	D SOLAR CELLS.	OF THE ABOVE DE	FECTS SHALL				
1. DELAMI 2. EXPOSE 3. CRACKE ALL ASSEMB	D SOLAR CELLS. BLIES HAVING ANY WORK OF SOLAR CE	LL ASSEMBLICS.				ED AFTED AL	ı TESTS
1. DELAMI 2. EXPOSE 3. CRACKE ALL ASSEMB	D SOLAR CELLS. BLIES HAVING ANY WORK OF SOLAR CE	LL ASSEMBLICS.				ED AFTER AL	L TESTS
1. DELAMI 2. EXPOSE 3. CRACKE ALL ASSEMB FOR ALL RE 007 CLEAN SOLA SPECIFIED	D SOLAR CELLS. BLIES HAVING ANY WORK OF SOLAR CE AR PANEL PER ITEM BY THE REE.	SO3 PRIOR TO F	FIRST FUNCTIO	NAL TEST AN	D AS REQUIR		
1. DELAMI 2. EXPOSE 3. CRACKE ALL ASSEMB FOR ALL RE 007 CLEAN SOLA SPECIFIED	D SOLAR CELLS. BLIES HAVING ANY WORK OF SOLAR CE AR PANEL PER ITEM BY THE REE.	SO3 PRIOR TO F	FIRST FUNCTIO	NAL TEST AN	D AS REQUIR		
1. DELAMI 2. EXPOSE 3. CRACKE ALL ASSEMB FOR ALL RE 007 CLEAN SOLA SPECIFIED	D SOLAR CELLS. BLIES HAVING ANY WORK OF SOLAR CE AR PANEL PER ITEM BY THE REE. TEST THE ELECTR	L ASSEMBLICS. 503 PRIOR TO F RICAL PERFORMANG	FIRST FUNCTIO	NAL TEST AN	D AS REQUIR	OIRECTION	-
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LOCKHEED MISSILES & SPACE COMPANY, INC.





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MODULE	/PLATE ASSY	(CONVENT	IONAL)		6216 86	MAR 0	7 1			PL_{x}	8517165	
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NAS3-2			N11-CL111-0	001-0	1X 06837) II \		J L . J .
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118	NOTE	FILLET 1. SOL PRE 2. APP 3. CUR	WIRES (ITE) VENT CLEAN -CLEANED Q LY ITEM 20 E 48 HRS M	M 204) SURFA -TIPS O IN A INIMUM	CES TO BE FILL AND AIR DRY 10 CONTROLLED MA	SURF ETED MINU NNER O DEGRE	FACE OF WITH JTES M.	F ITEM. ITEM 20 INIMUM	001 PER 03 (2-PRC	ITE PAN	M 502 AS FOLLOWS	
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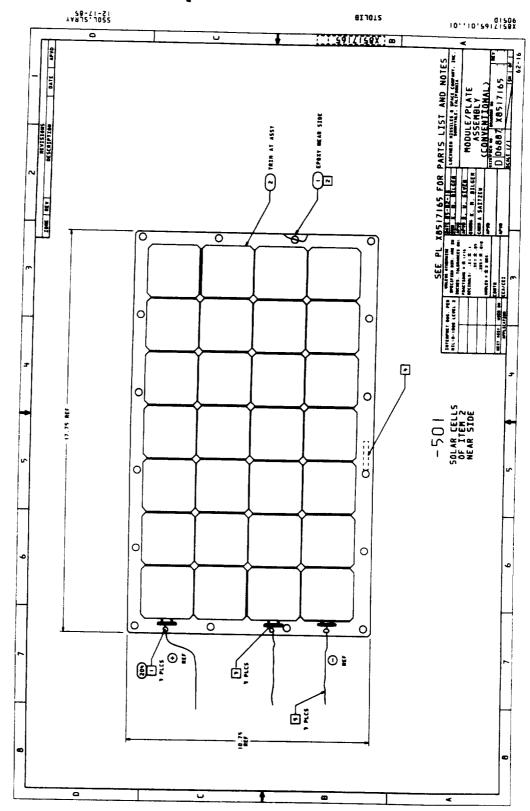
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LOCKHEED MISSILES & SPACE COMPANY, INC.

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NTRACT NUMBER		AUTHORITY		FSCM NO	MAR 07 21	E		ERING PARTS	LIST
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	3•	BONDLINE	THICHNESS SI	HALL BE .005	IDGE IN MORE	THAN ONE PLA	CE BETW	EEN ANY 2	
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						usins i	TEM 205	i _	
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003 2004	_								
004 LOCA	AL NOTE: MA	RK PART NO.	PER ITEM 5	05 APPROX A	3 3110 #144				
		5 1 5400	CHOWN SHOUL	D BE APPROX	3 FT. LONG.				
005 LOCA	AL NOTE: SI	NGLE LEADS	240#W 21100E				- ****	. N.C. •	
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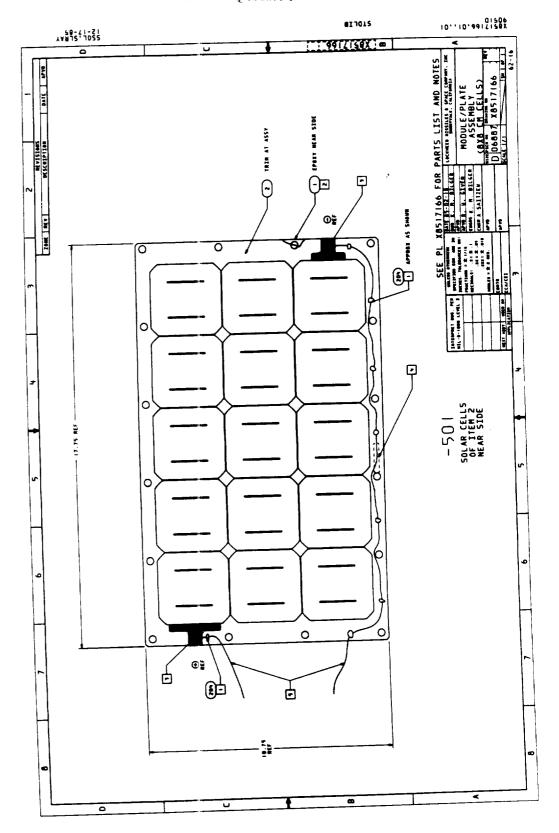


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04	A∺	,		MD920-22-4			SOLDER	SN63 WRMAP 2 OR 3	
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00	×			1421331			GEN ELEC SULDER	SOLDER PER	Ν
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APPENDIX B

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MODULE CAPACITANCE AND RESISTANCE

- I. Normal Orientation, 28 cells
 Use 55 mils silica/epoxy on aluminum
 Approx 2250 pf
 Approx 1.4 x 10¹¹ ohms
- II. Upside Down Orientation, 28 cells, 6 mil covers
 Use 50 mils silica/epoxy on aluminum
 Approx 2250 pf
 Approx 1.5 x 10¹¹ ohms

NORMAL CELL ORIENTATION

I. Materials Properties

MATERIAL	DIELECTRIC CONSTANT	VOLUME RESIVITY	DIELECTRIC STRENGTH
	in ε _ο	Ω - cm	volts/mil
Silicone Kapton Epoxy Silica	4.3 to 3.4 3.9 to 3.5 5.2 to 2.8 3.8	10 ¹⁴ to 10 ¹⁶ 10 ¹⁵ to 10 ¹⁶ 10 ¹⁴ to 10 ¹⁶ 6.3 x 10 ¹⁴	400 to 700 310 to 560 400

II. Capacitance (~DC)

Find capacitance on a per cell basis (34.8 cm^2)

Let C, be 25% of area, $C_2 = 75\%$ of area

MODULE, UPSIDE DOWN ORIENTATION

- I. Material same as "Normal Cell Orientation" Assume all ϵs = 3.8 $\epsilon_{\rm O}$ for silica/epoxy, silicones
- II. Capacitance (~DC)

On a per cell basis

_____ Cell

3 mils silicone

6 mils microscheet or quartz ε = 4.610¹⁵ Ω-cm

$$C = \frac{\varepsilon \varepsilon_0 \text{ Area}}{d} = \frac{3.9 \times 3.85 \times 10^{-14} \text{ farads/cm} * 34.8 \text{ cm}^2}{(3 + 6 + X) * 0.00254 \text{ cm/mil}}$$

$$C = \frac{4729}{(9 + \chi)} \text{ pf per cell}$$

Module capacitance = 28 * cell capacitance

2000 to 2500 pf =
$$28 * \frac{4729}{(9 + X)}$$
 pf

71 to 89 =
$$\frac{4729}{9 + X}$$

$$\chi = \frac{4729}{71 \text{ to } 89} - 9$$

2000 to 2500 pf =
$$X = 58$$
 mils to 44 m² ls silica/epoxy

III Resistance

Resistance =
$$\frac{10^{15} \ \Omega - cm \ (X + 9)mils * 0.00254 \ cm/mil}{28 \ cells * 34.8 \ cm^{2}/cell}$$

Resistance = $2.607 \times 10^9 * (X + 9)$ mils

for
$$X = 58$$
 $R = 1.75 \times 10^{11} \Omega s$ $X = 44$ $R = 1.38 \times 10^{11} \Omega s$

Cper cell = .25C₁ + .75C₂ or =
$$\left(\frac{1151}{(2+X)_{mils}} + \frac{3453}{(3+X)_{mils}}\right)$$
 pico farads per cell

Module capacitance = 28 * cell capacitance

So 2000 to 2500 pico farads = 28
$$\star \left(\frac{1151}{(2 + X)_{mils}} + \frac{3453}{(3 + X)_{mils}} \right)$$
 pico farads

or (1) (2) 71 to 89 =
$$\frac{3453 + 1151x + 6906 + 3453x}{6 + 5x + x^2}$$
 = $\frac{10359 + 4604x}{6 + 5x + x^2}$

(1)
$$X^2 - 59.8 \times -140.0 = 0 \rightarrow x = 62, -4.5 \text{ mils}$$

(2)
$$X^2 - 46.7X - 110.4 = 0 \rightarrow x = 49, -4.5 \text{ mils}$$

$$X = silica/epoxy$$
 $\begin{cases} X = 62 \text{ mils at } 2000 \text{ pf} \\ X = 49 \text{ mils at } 2500 \text{ pf} \end{cases}$

III. Resistance

Assume average of >10 15 Ω -cm restivity for silica/epoxy then,

Resistance =
$$\frac{10^{15} \Omega - cm * (X mils) * 0.00254 cm/mil}{28 cells * 34.8 cm^{2}/cell}$$

Resistance =
$$2.607 \times 10^9 \times (X \text{ mils})$$

for X = 62 mils R = 1.62 x
$$10^{11} \Omega s$$

X = 49 mils R = 1.28 x $10^{11} \Omega s$

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